

RESEARCH ON UNDERFLOOR DUCTED HEATING HOUSES WITH AIR-BASED PVT PANEL ON THE ROOFS

~INVESTIGATION OF COST-EFFECTIVE FOUNDATION INSULATION SPECIFICATIONS~

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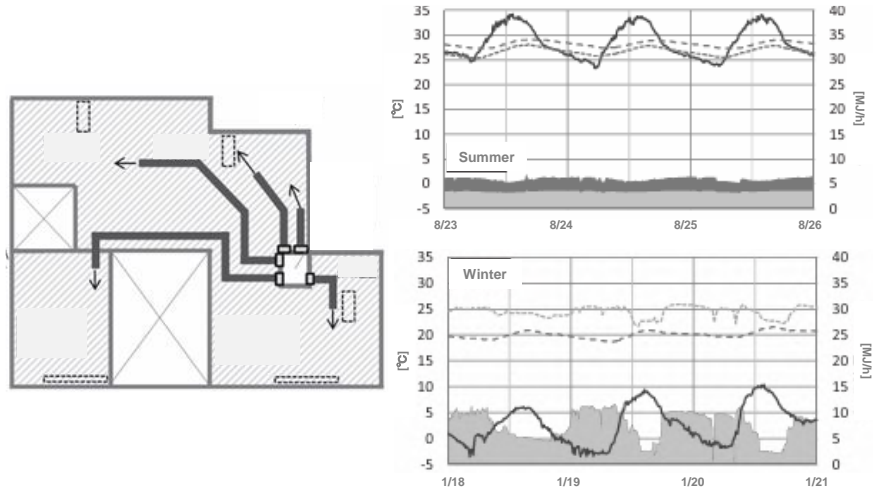
*4 OM Solar Inc., Japan

*5 Tokyo University of Science, Japan

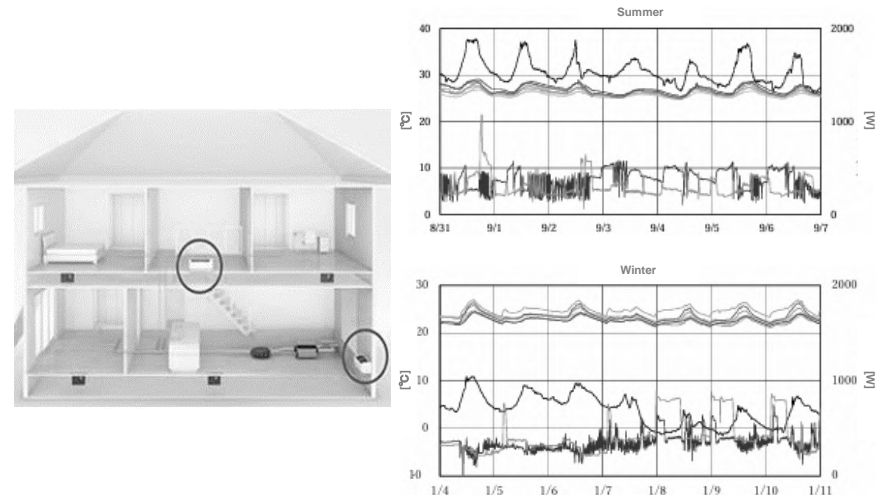
*6 Tokyo University, Japan

Research background

Demand for comfort, health, and energy conservation in housing has increased, and many houses are being built with insulation performance that exceeds energy conservation standards.



Demonstrated the effectiveness of floor chamber air conditioning in the highly insulated detached house.¹⁾

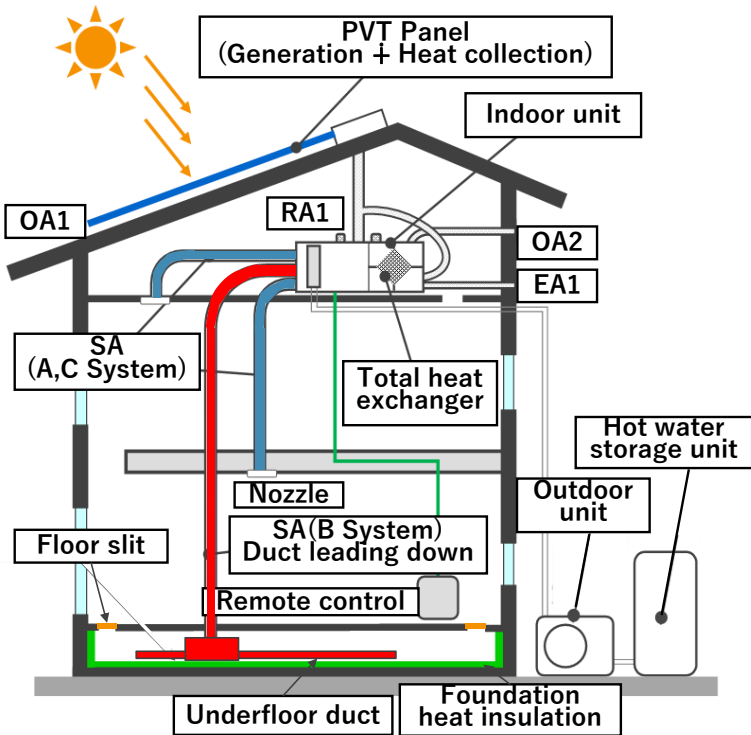


The good indoor environment can be achieved in the ductless whole-house air conditioning system using the wall-mounted air conditioner²⁾

In the detached house with the large floor area, the temperature difference between rooms is expected to be large, and the ductless whole-house air-conditioning system may not be sufficient to ensure the comfortable thermal environment.

- 1) : Iguchi, M., et al. : Verification of Air Distribution Thermal Environment and Energy Consumption in an Existing Detached House
A methodology for designing the air-conditioning system using floor-chambers in a residence Part 4.
- 2) : Iwasaki, Y., et al. : Study on a Ductless Central Air-conditioning System Utilizing Crawl Space as Supply Chamber
Part 1 Overview of the System and Verifications by Measurements, technical papers of annual meeting.

Whole-house air conditioning system under study



System overview

System specification

| Type | Item | Data |
|------------------|---|-------|
| Heating | Standard heating capacity[kW] | 4.0 |
| | Standard power consumption for rated heating[kW] | 0.905 |
| | Rated low-temperature heating capacity[kW] | 4.7 |
| | Rated low-temperature heating power consumption[kW] | 1.700 |
| Air volume | Coefficient of Performance(COP)[-] | 4.42 |
| | Rated supply air fan airflow[m ³ /h] | 930 |
| Ventilation | Rated power consumption of indoor blower fan[W] | 215 |
| | Rated ventilation airflow[m ³ /h] | 200 |
| | Rated power consumption[W] | 65 |
| | Temperature exchange efficiency[%](winter) | 90 |
| Hot water supply | Total heat exchange efficiency[%](winter) | 85 |
| | Tank capacity[L] | 370 |
| | Winter peak power consumption[kW] | 1.35 |
| | Intermediate period standard power consumption[kW] | 1.06 |

The ducted air-conditioning system under the floor (hereinafter referred to as "this system") was studied, which is expected to realize the thermal environment with less temperature difference between rooms by uniformly heating the under-floor space through the use of under-floor ducts.

This system is also expected to reduce the heating load by using HP (Heat Pump) and roof PVT (PhotoVoltaic and Thermal collectors) panels together.

This system is designed for continuous operation, heat capacity of the foundation is not expected, and full insulation over the earthen floor is the standard installation method. However, this installation method is **time-consuming and expensive**.



< Research purpose >

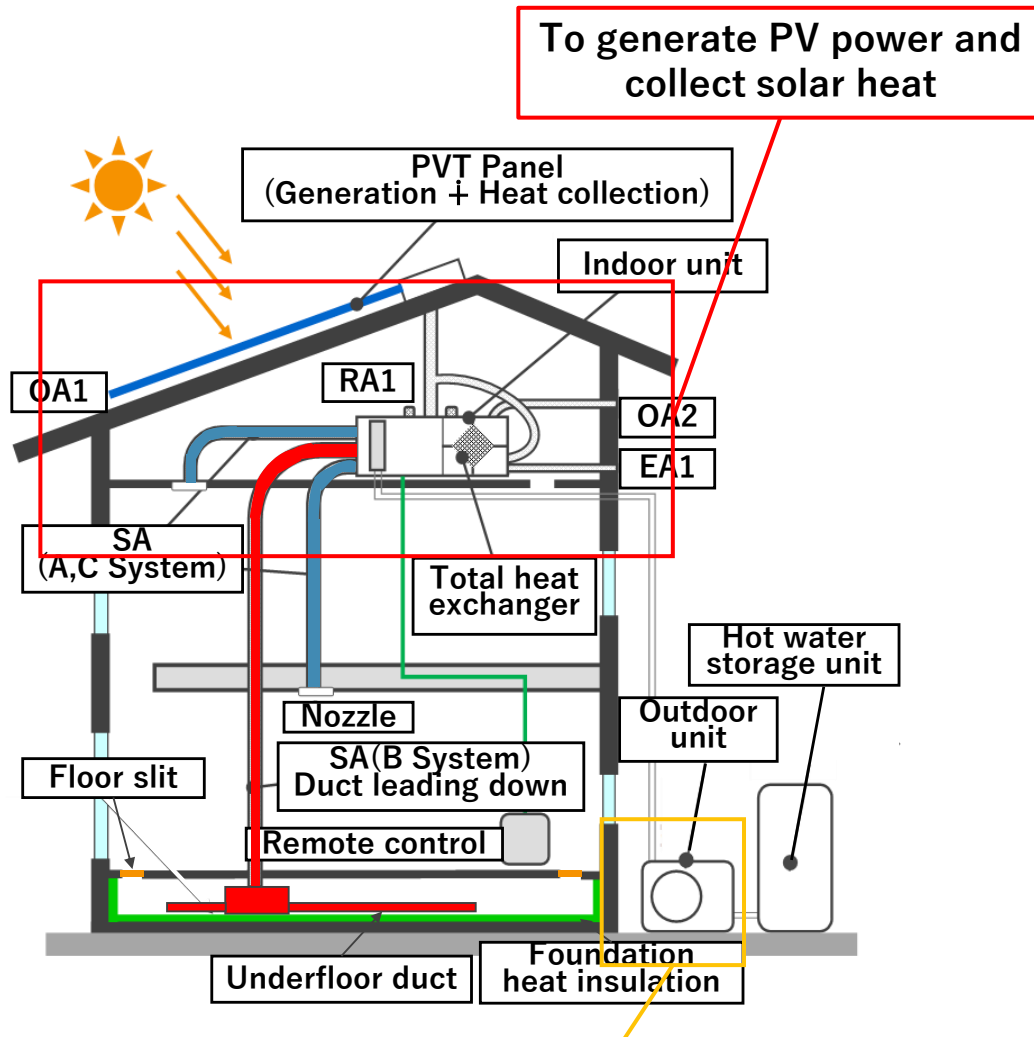
1. To understand the amount of under-floor heat loss
2. To calculate effective target values for foundation insulation performance



In this study, the following items were compared using simulations

- The thermal environment
- Underfloor heat loss
- Cost

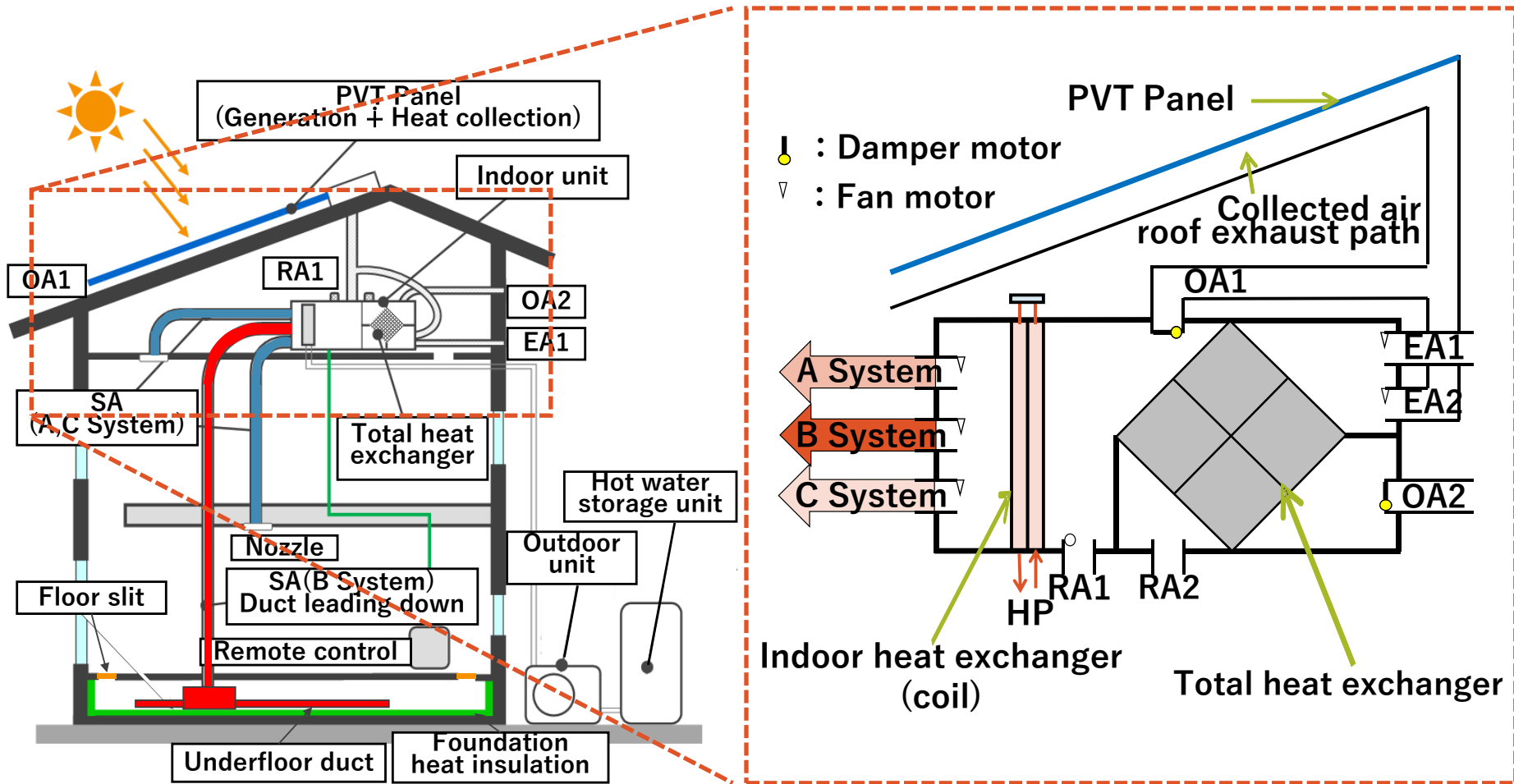
System overview



A single HP to heat/cool and supply hot water

Simultaneous operation with heating is not possible, and priority is given to hot water heating

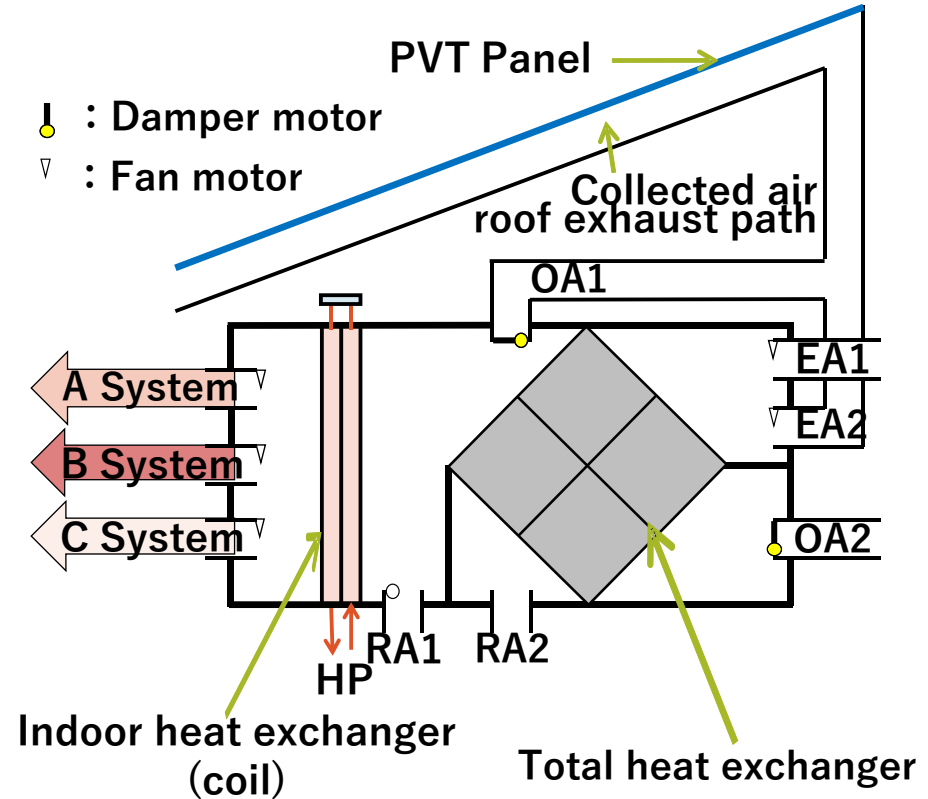
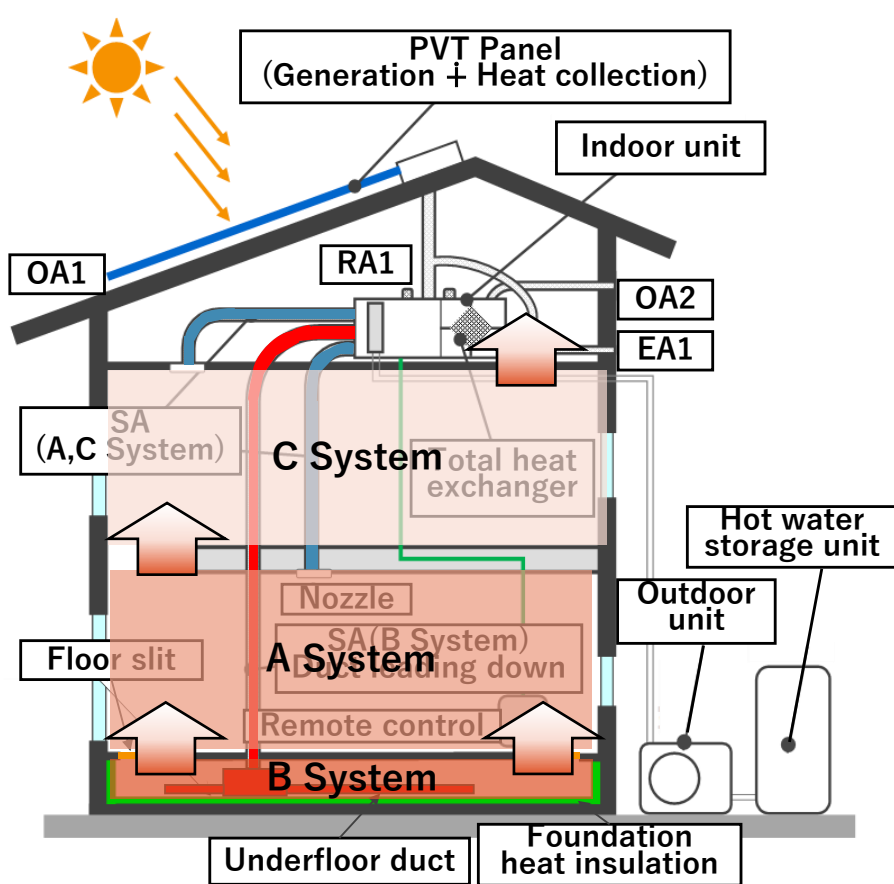
System overview



The indoor unit of this system has the built-in total heat exchange ventilation.

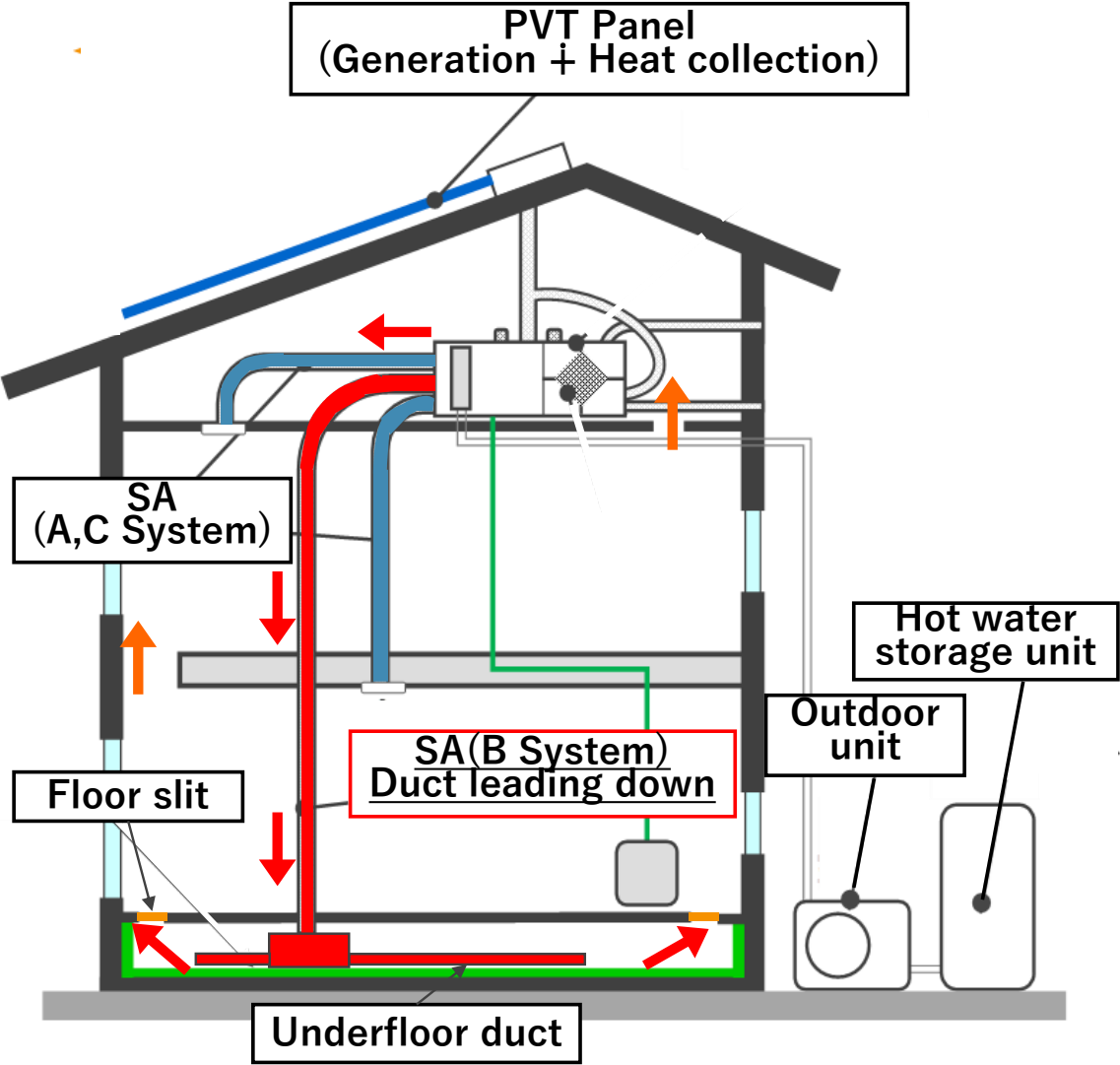
System overview

- A system : 1st floor B system : Under floor C system : 2ed floor



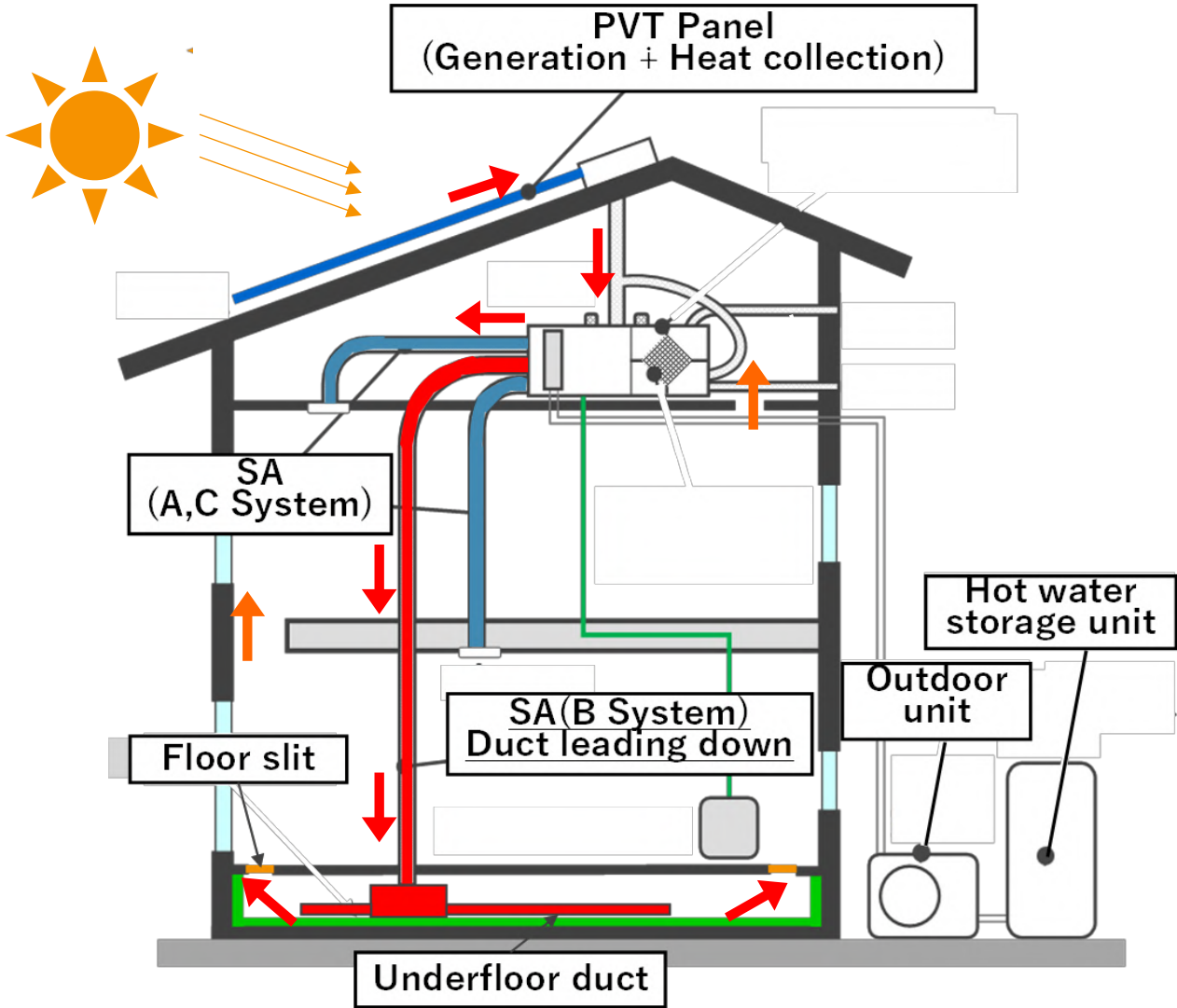
Supplied air is then returned to the indoor unit installed in the back of the shed through the ceiling vents via the atrium and stairwell and circulates throughout the dwelling unit.

System overview in winter



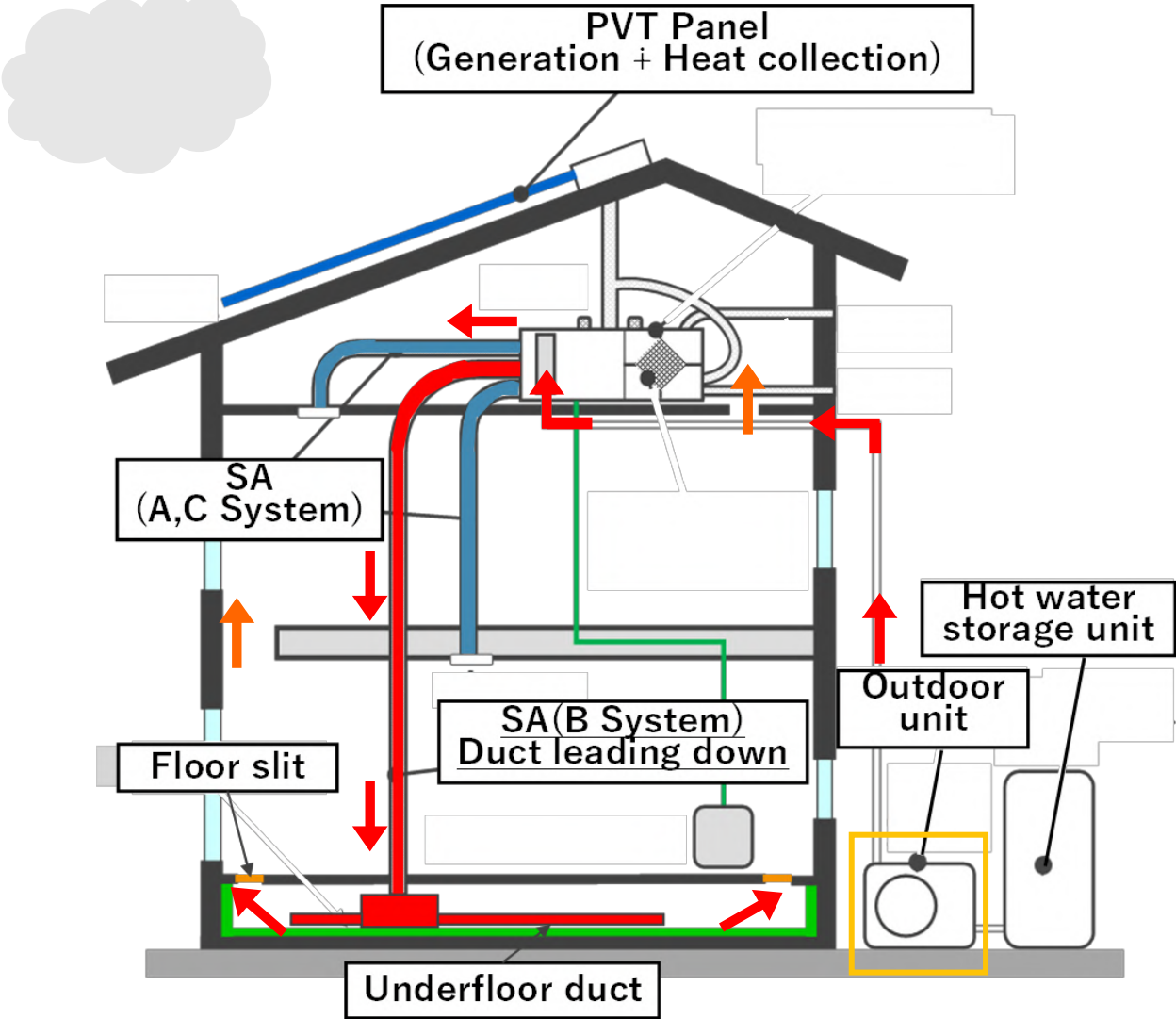
In winter, warm air is supplied under the floor mainly from the B system and blown into the room from each floor slit.

System overview in winter



On sunny days, heating is provided by solar heat collection by PVT panels, and if the amount of collected heat is insufficient, it is supplemented by HP heating.

System overview in winter



At night and on cloudy days, heating is provided by HP.

1. Introduction

- Research background and purpose
- System overview

2. Construction of simulation method to reproduce this system

- Reproduce this system behavior and organize simulation conditions
- Consistency verification from simulation results

3. Case study with simulation

- Calculate cost-effective foundation insulation performance for underfloor heating based on comparison of thermal environment, underfloor heat loss, and cost

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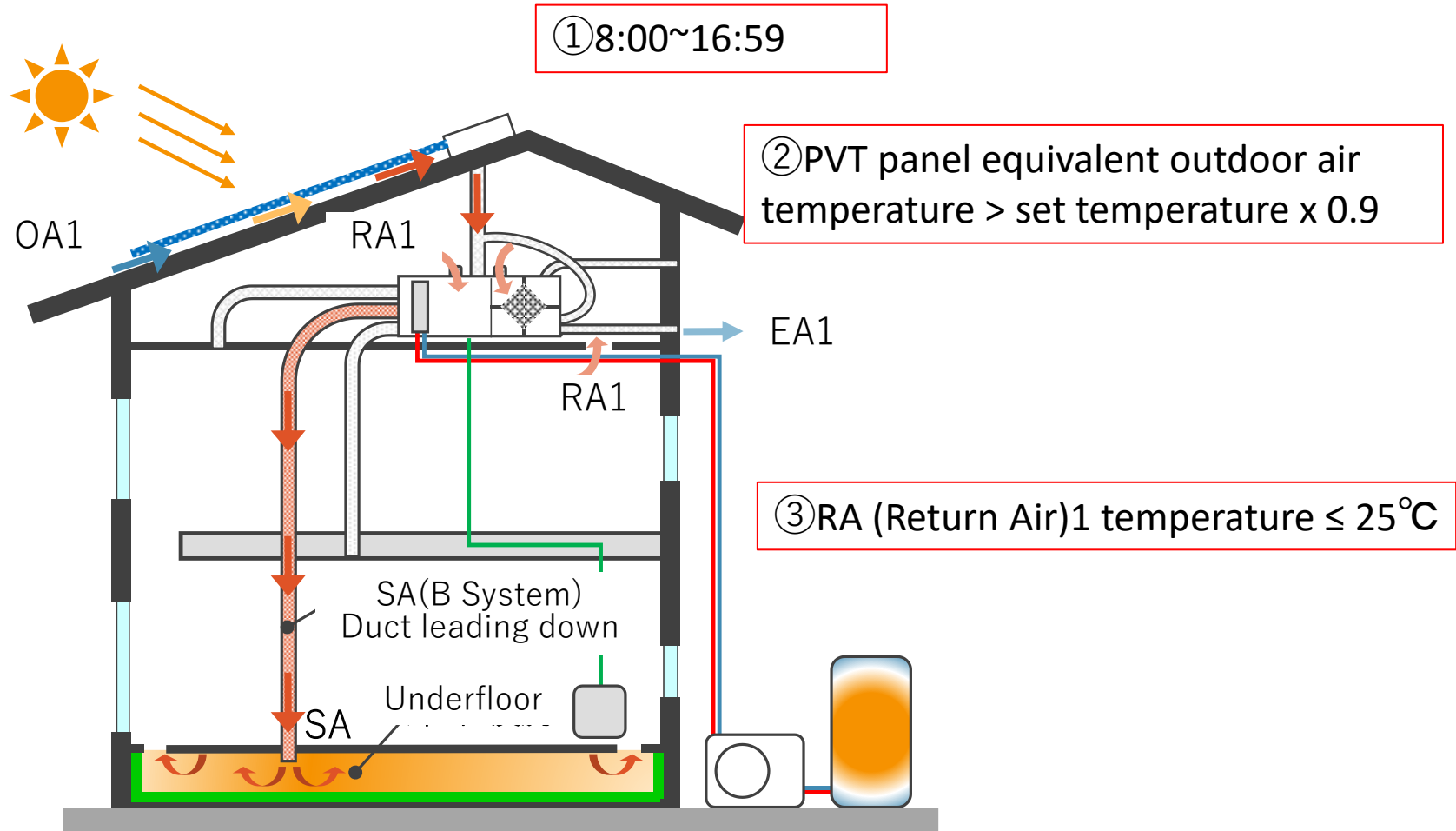
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Heating operation control in this study



The operating conditions for solar heating were defined as when conditions ①②③ were met. In estimating the heat collection temperature of the PVT panels and the amount of electricity generated by the PV panels, calculations were made based on previous studies^{1) 2)}

- 1) Udagawa, M., et al. : Simulation of roof integrated solar collector for space and DHW heating systems, Part 1 Simulation model, technical papers of annual meeting.
- 2) Satoh, M., et al. : Simulation of roof integrated solar collector for space and DHW heating systems, Part 2 Example results of space and DHW heating system for residential house using solar air collector, technical papers of annual meeting.

Calculation of under-floor heat loss in this study

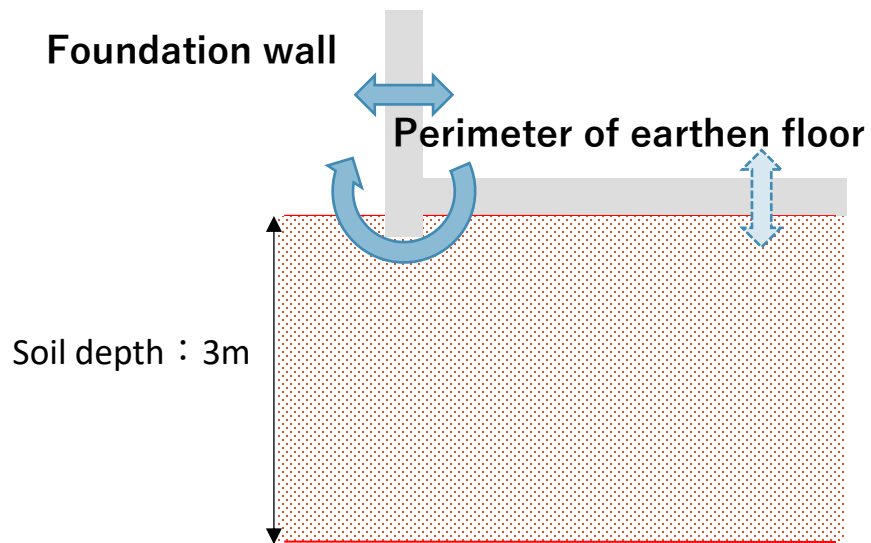
<Calculation Methods in Calculation Methods in this Study>

Heat Transfer Calculation

- 2D steady heat conduction

Soil properties

- Thermal conductivity : $1.0\text{W}/(\text{m} \cdot \text{K})$



*** No heat loss calculation for the center of earthen floor**

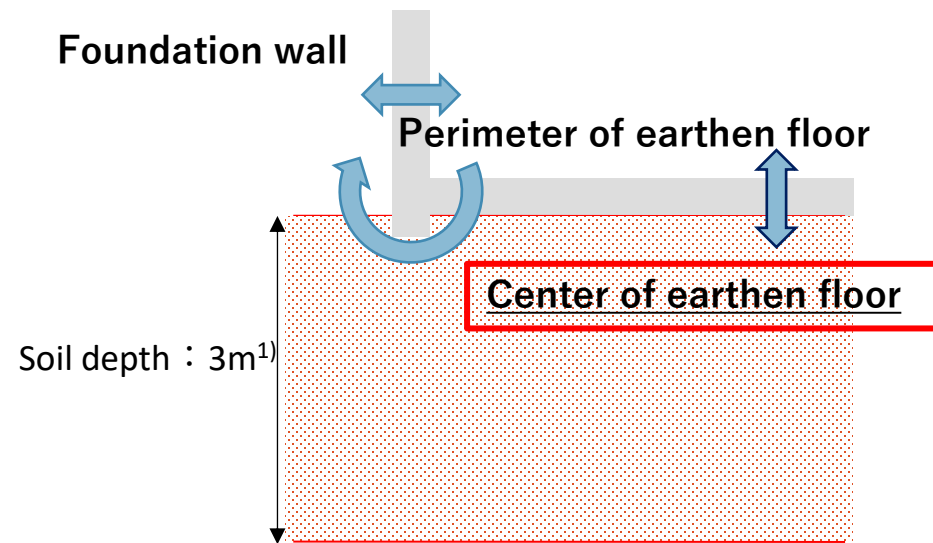
<Calculation Methods in this Study>

Heat Transfer Calculation

- 1D unsteady heat conduction

Soil properties

- Thermal conductivity : $1.0\text{W}/(\text{m} \cdot \text{K})$
- Specific heat by volume : $3340\text{J}/(\text{m}^3 \cdot \text{K})^2$



Soil boundary temperature conditions :
Annual average outdoor temperature¹⁾

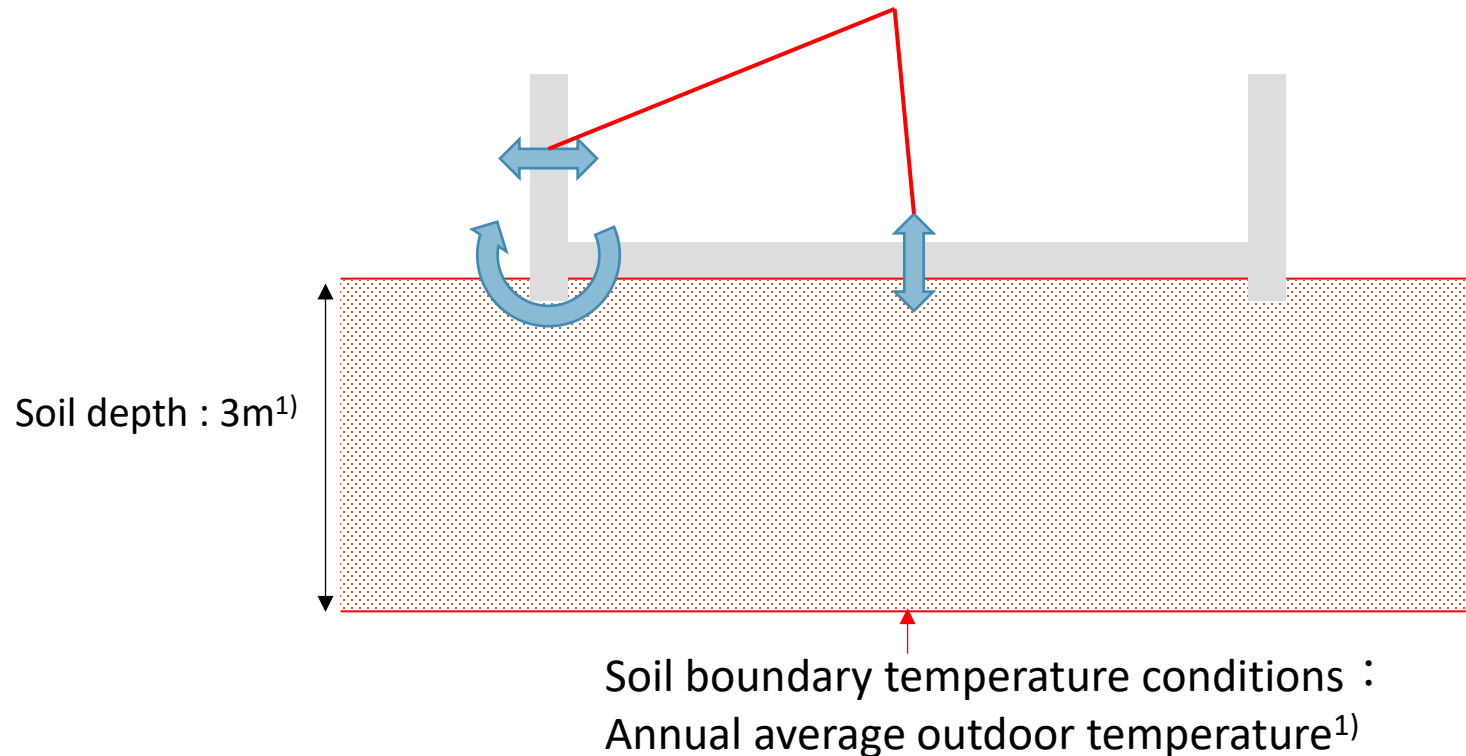
1) Satoh, M., et al. : Study on the evaluation method of heat transfer via the ground on detached houses with insulated foundation, technical papers of annual meeting
2) The Society of Heating, Air-Conditioning and Sanitary Engineers of Japan : Try and Learn Thermal Load HASPEE, 2012.

Calculation of under-floor heat loss in this study

Aiding period¹⁾ 1 year in this study

Soil properties²⁾ Thermal conductivity : $1.0\text{W}/(\text{m} \cdot \text{K})$
Specific heat by volume : $3340\text{J}/(\text{m}^3 \cdot \text{K})$

**Foundation wall & Center of earthen floor :
1dimentional unsteady heat conduction**



Soil boundary temperature conditions :
Annual average outdoor temperature¹⁾

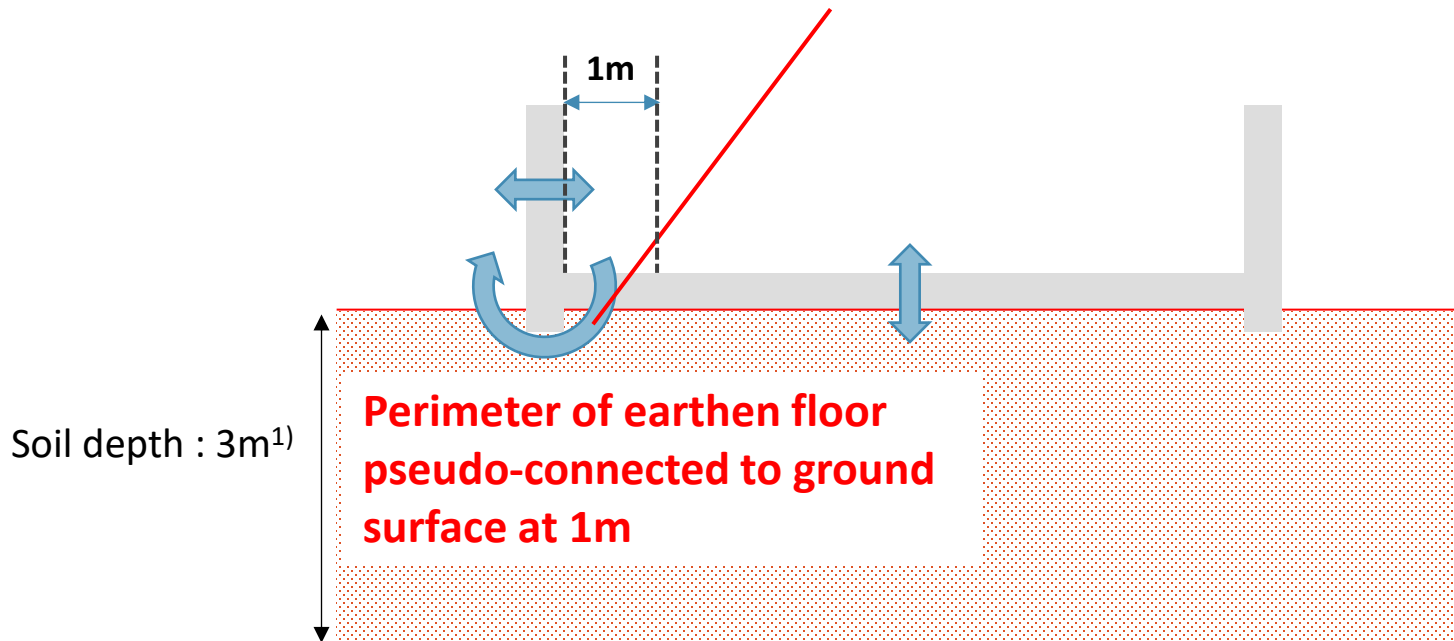
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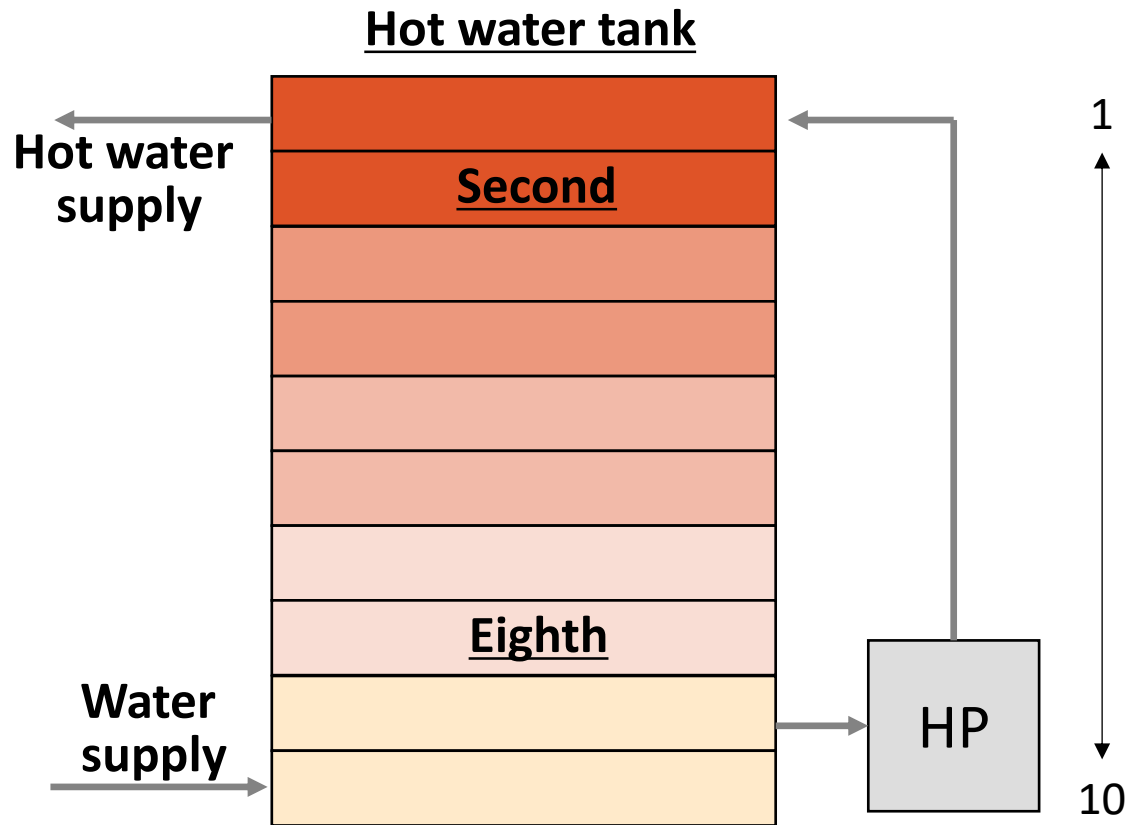
**Perimeter of earthen floor :
Approximated by 1dimentional unsteady heat conduction**



1) Satoh, M., et al. : Study on the evaluation method of heat transfer via the ground on detached houses with insulated foundation, technical papers of annual meeting

2) The Society of Heating, Air-Conditioning and Sanitary Engineers of Japan : Try and Learn Thermal Load HASPEE, 2012.

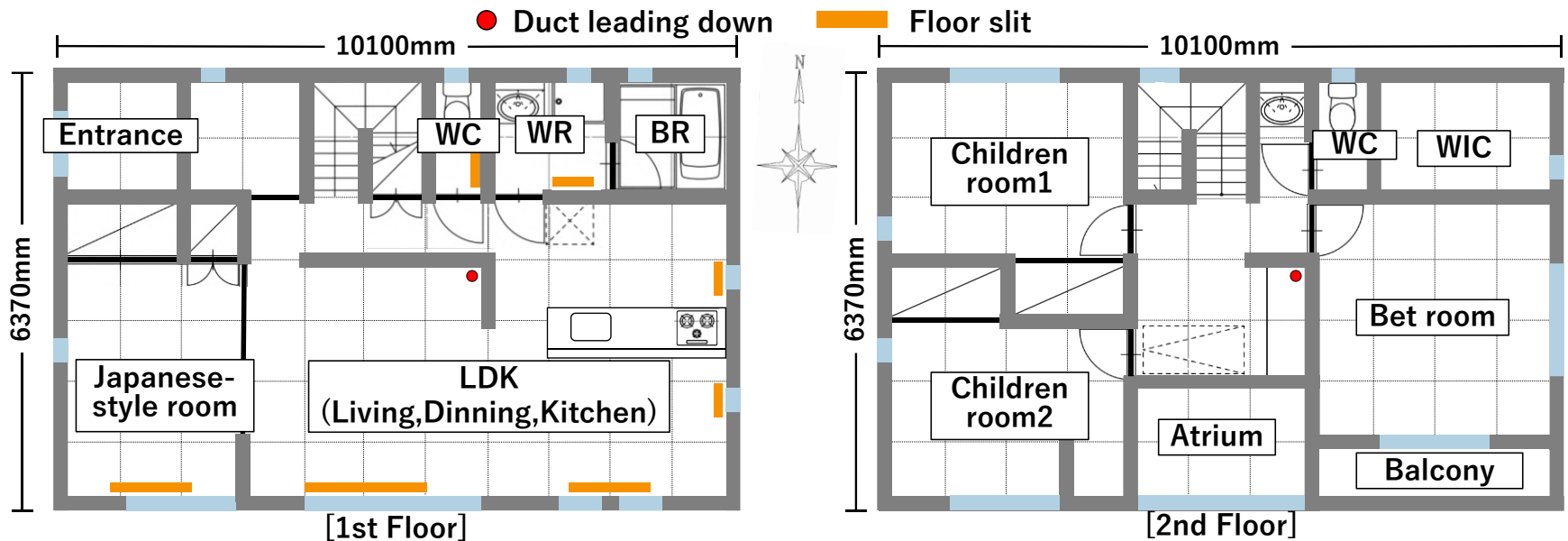
Hot water supply operation control in this study



The storage tank was divided into 10 blocks, and the control model was set up so that HP hot water heating would start and HP heating would stop when the eighth block fell below 65°C from 12:00 to 15:59 or when the second block fell below 45°C from 20:00 to 23:59.

Building outline

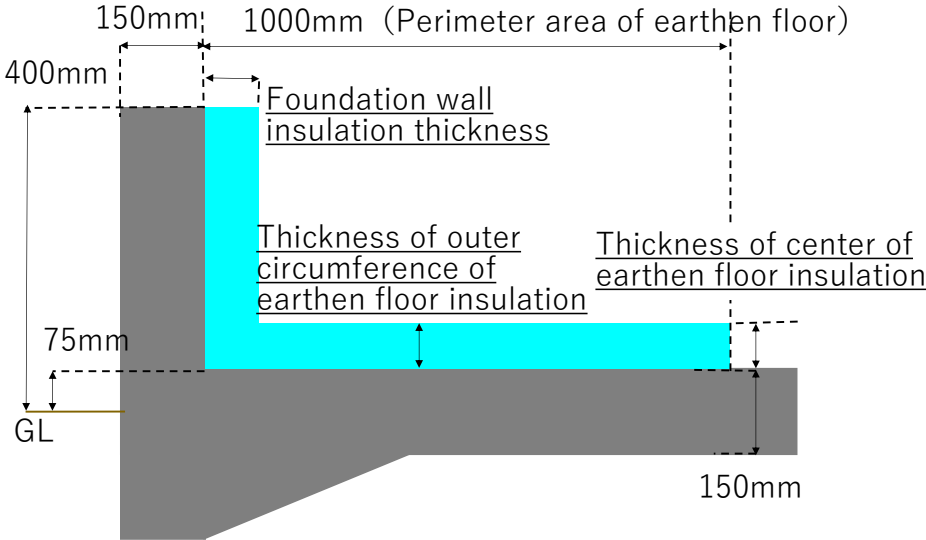
| Type | Data |
|---|--------------------------|
| Building Model | Passive standard plan |
| Building Structure | Two-story wooden house |
| Roof[Method/Slope(cm)/Eaves length(mm)] | Gable roof/12.1/600 |
| Address | Tokyo 23 wards(Region 6) |
| U_A value/ η_{AC} value | 0.46/1.9 |
| PVT panel(kW) | 8.2 |
| U value(W/m^2K)[Roof/Wall/ Window] | 0.13/0.39/2.33 |



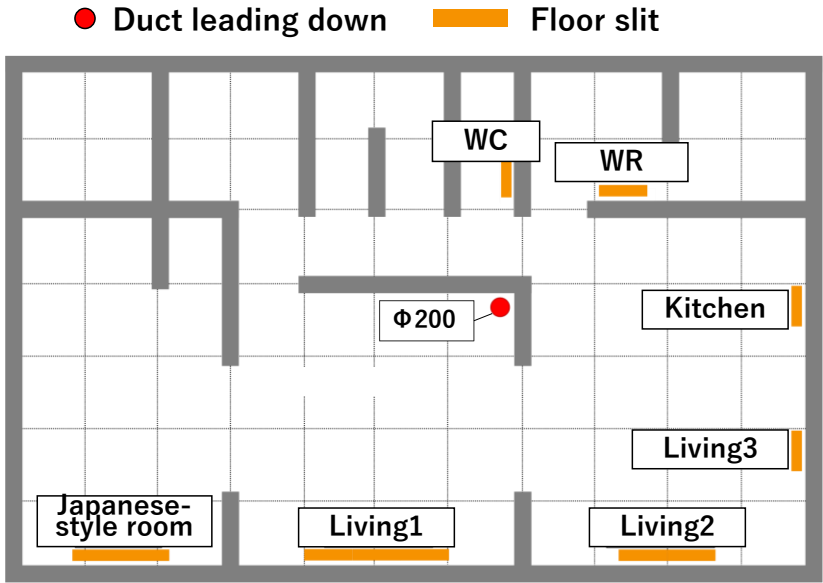
Using passive standard plans ¹⁾ that are common in the shape and scale of the houses.

1) Taniguchi, K., et al. : New Passive Standard Plan Proposal, Self-Sustaining Circulation Project Symposium, 2020.

Simulation building outline



Cross section of foundation



Underfloor plan

The foundation insulation material is extruded polystyrene foam insulation type 3 bA ($\lambda = 0.028 \text{ W/mK}$).

Thermal network calculation conditions

| Type | Data |
|---|---|
| Thermal network calculation software | EESLISM7.2 |
| Meteorological data | Standard year extended AMeDAS weather data 2010 Tokyo |
| Analysis period and interval | 10/1~4/31(preparatory period : 1year) · 1hour |
| Ventilation operation | Air volume : always 200m ³ /h Temperature exchange efficiency : 85% |
| Solar heating operating conditions | 8:00~16:59 PVT equivalent outside temperature > Set temperature × 0.9 Return air temperature ≤ 25°C |
| HP hot water heating operating conditions | Dividing the hot water storage tank into 10 blocks, the 8th is less than 65° C at 10:00~14:00 or the 2nd is less than 45° C at 20:00~24:00 |
| Conditions of use for hot water supply | Based on the energy conservation standard M1 standard 4-person mode weekday (medium) |
| Internal heating conditions | Based on criteria for residential project builders |

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- The weader data used was the standard year extended AMeDAS weader data 2010 Tokyo.
- For ventilation operation, the ventilation rate of 200 m³/h was always, and the temperature exchange efficiency of 85% was used.

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- The operating conditions for heating and hot water heating were reproduced from this system's controls, while other settings were made assuming general conditions.

CFD Analysis conditions(Used as part of thermal network calculations)

| Type | Data |
|--------------------------------------|--|
| Analysis software | FlowDesigner2022 |
| Total number of meshes | 5.8 million mesh |
| Turbulence model | Standard k- ε model |
| Convergence criterion | (stationary) $1.0 \times 10^{-3.5}$ |
| Outside temperature/Soil temperature | -0.3°C/18.6°C |
| Inflow conditions (SA from B system) | Airflow : 437m ³ /h Blowoff temperature : 49.3°C |
| Outflow conditions (RA) | 437m ³ /h from unit location |

- The outdoor air temperature was set to the lowest outdoor air temperature in January of the standard year's extended AMeDAS weather data.
- The soil temperature was set to the annual average outdoor air temperature of the standard year's AMeDAS weather data.

CFD Analysis(Used as part of thermal network calculations)

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|--------------------------------------|---|
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| Outflow conditions (RA) | 437m ³ /h from unit location |

- The blowout temperature was calculated using the following formula, assuming an indoor temperature of 22°C.

$$t_D = t_R + \frac{q_s}{0.34 \times Q_{AC}}$$

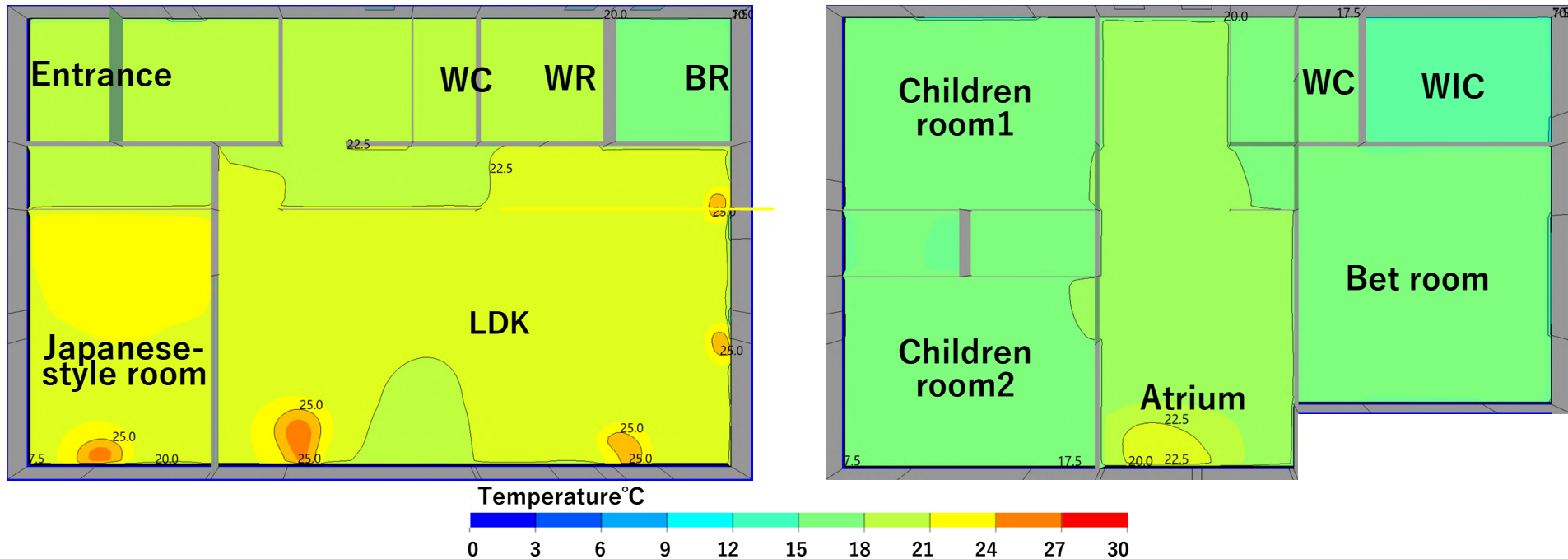
t_D : Blowoff temperature[°C] t_D : Indoor temperature[°C]
 q_s : Maximum heat load determined by thermal network calculation[W]
 Q_{AC} : Airflow[m³/h]

Simulation results

- Room temperature distribution

1st Floor

2ed Floor

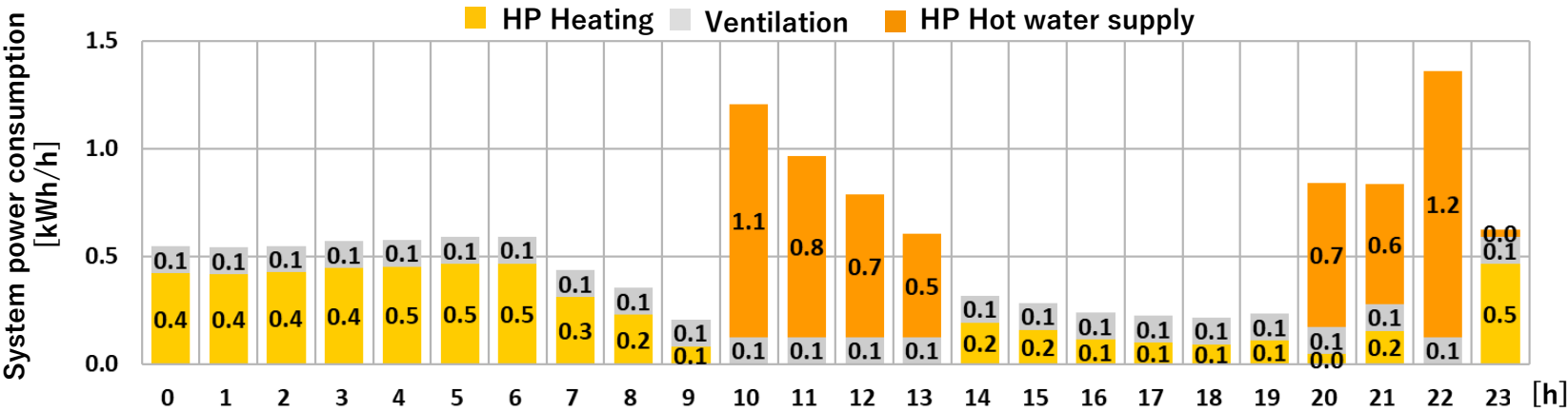
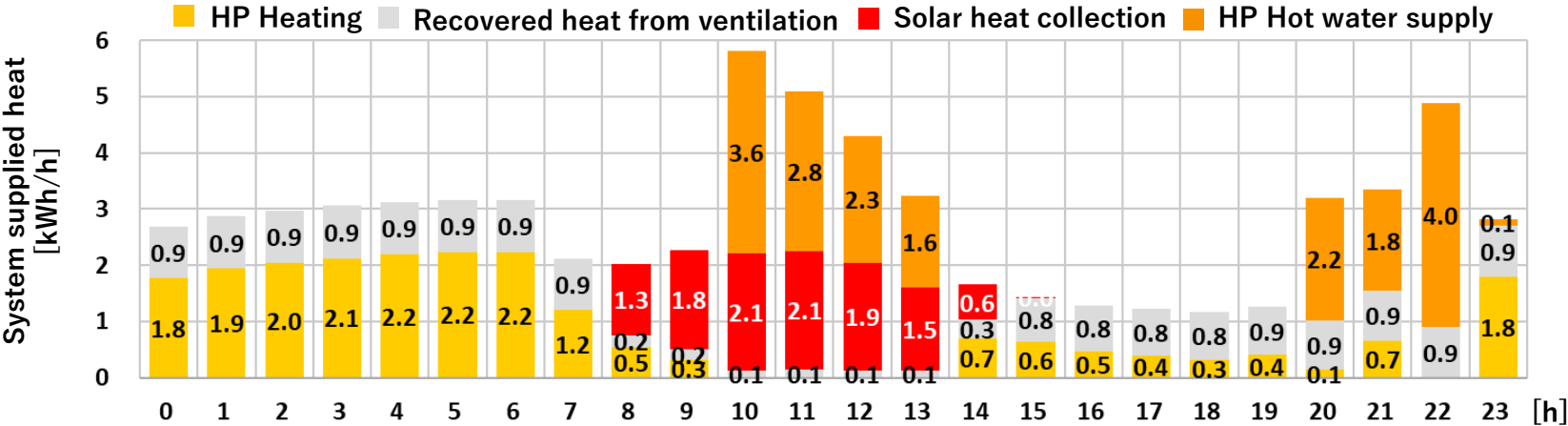


the room temperature in LDK is about 23°C, which is around the set temperature of 22°C.

→ This was judged to be generally appropriate and set on thermal network calculations.

Simulation results

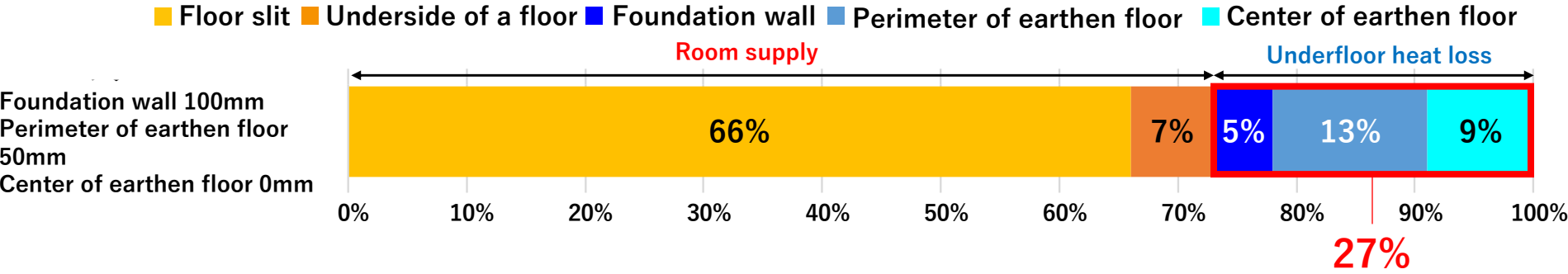
- Average system supplied heat and power consumption by time of day in January



During the daytime, the HP is used to heat water supply, and the heating is done only by solar heat collection, and no heating power consumption was generated by HP.

Simulation results

- Percentage of heat supplied under the floor to be allocated to



The amount of heat loss under the floor in relation to the amount of heat supplied under the floor was **5% for the foundation wall, 13% for the perimeter of the earthen floor, and 9% for the center of the earthen floor.**

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In this section the authors look at the impact of differences in basic thermal insulation performance targeting energy conservation region classifications 5 and 6.

Region5(Sendai)



Grade4

Grade5



Thermal insulation performance
12Case

Region6(Tokyo)

Grade6

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Region5(Sendai)

Region6(Tokyo)



Grade4









Grade5

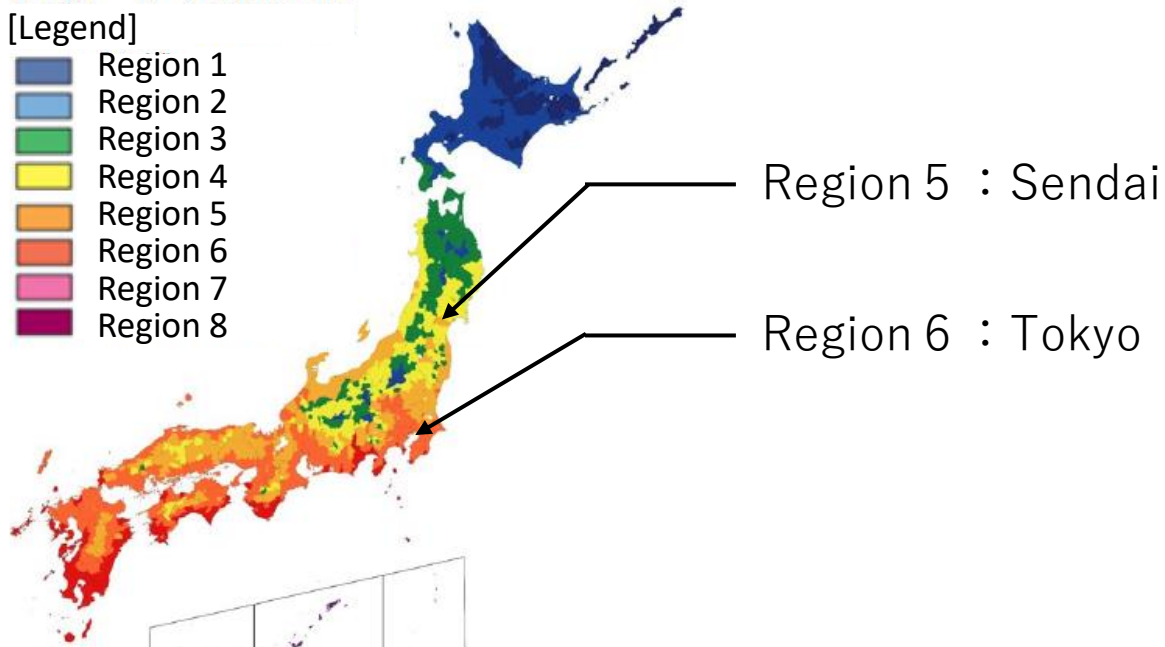
Grade6



Thermal insulation performance
12Case

[Legend]

-  Region 1
-  Region 2
-  Region 3
-  Region 4
-  Region 5
-  Region 6
-  Region 7
-  Region 8



Targeting Tokyo in region 6 and Sendai in region 5

In this section the authors look at the impact of differences in basic thermal insulation performance targeting energy conservation region classifications 5 and 6.

Region5(Sendai)



Grade4

Grade5

Grade6



Thermal insulation performance
12Case

Region6(Tokyo)

| Insulation grade(U_A value) [W/m ² K] | Region 5(Sendai) | Region 6(Tokyo) |
|---|------------------|-----------------|
| Grade 2 | 1.67 | 1.67 |
| Grade 3 | 1.54 | 1.54 |
| <u>Grade 4</u> | <u>0.87</u> | <u>0.87</u> |
| <u>Grade 5</u> | <u>0.60</u> | <u>0.60</u> |
| <u>Grade 6</u> | <u>0.46</u> | <u>0.46</u> |
| Grade 7 | 0.26 | 0.26 |

In Japan, insulation **grade 4** is used as the value for energy conservation standards.

In this section the authors look at the impact of differences in basic thermal insulation performance targeting energy conservation region classifications 5 and 6.

Region5(Sendai)

Grade4

Grade5

Grade6

Thermal insulation performance
12Case

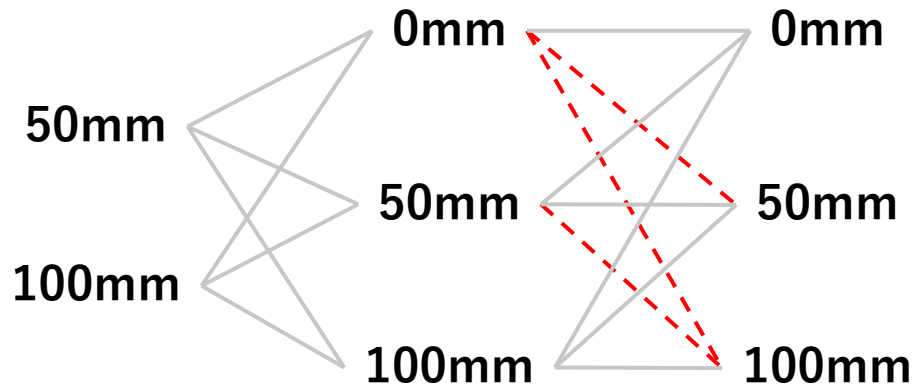


Region6(Tokyo)

Foundation
wall

Perimeter
of earthen floor

Center
of earthen floor

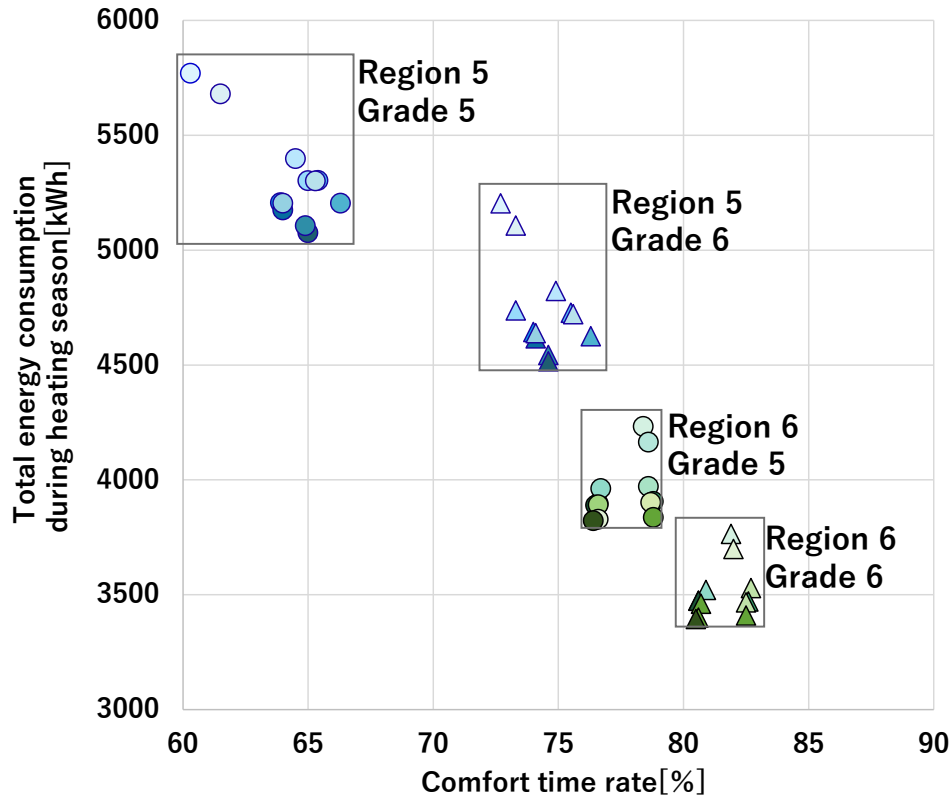


Foundation insulation performance, 12 cases were considered, excluding the red line.

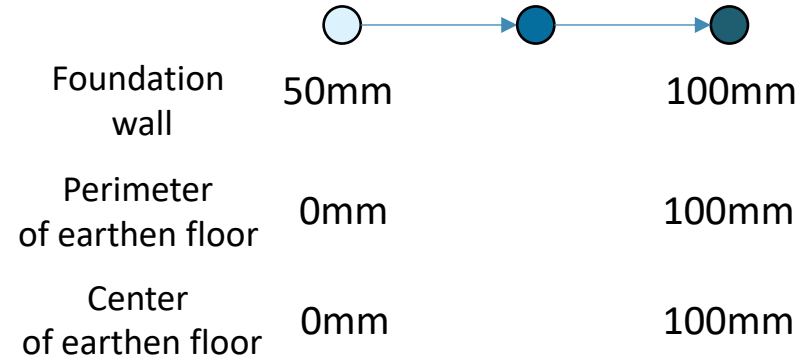
Energy consumption and comfort considerations

$$C_{time} = \frac{OT_{20\sim24}}{d \times 24 \times r} \times 100[\%]$$

C_{time} : Comfort time rate d : Number of days of period covered r : Number of target rooms(Living room, etc.)
 $OT_{20\sim24}$: Number of hours within the target room operating temperature of 20~24° C



- ○ Grade5 △ Grade6
- Blue Region5(Sendai) Green Region6(Tokyo)
- As the insulation becomes thicker, the color is made darker.

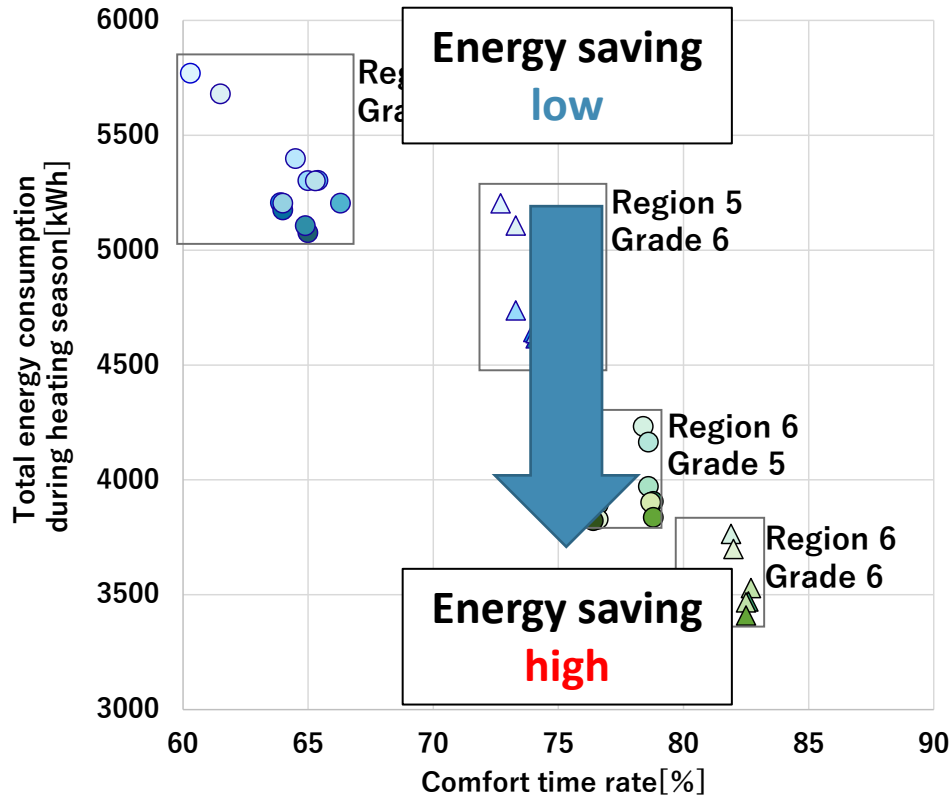


The comfort time rate was defined using the above equation with a comfort temperature range of 20-24°C.

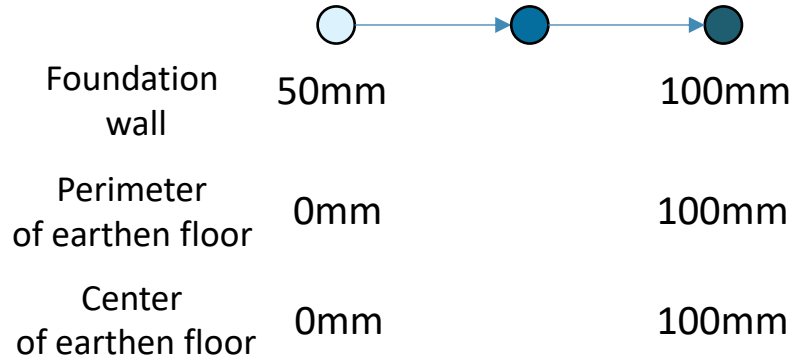
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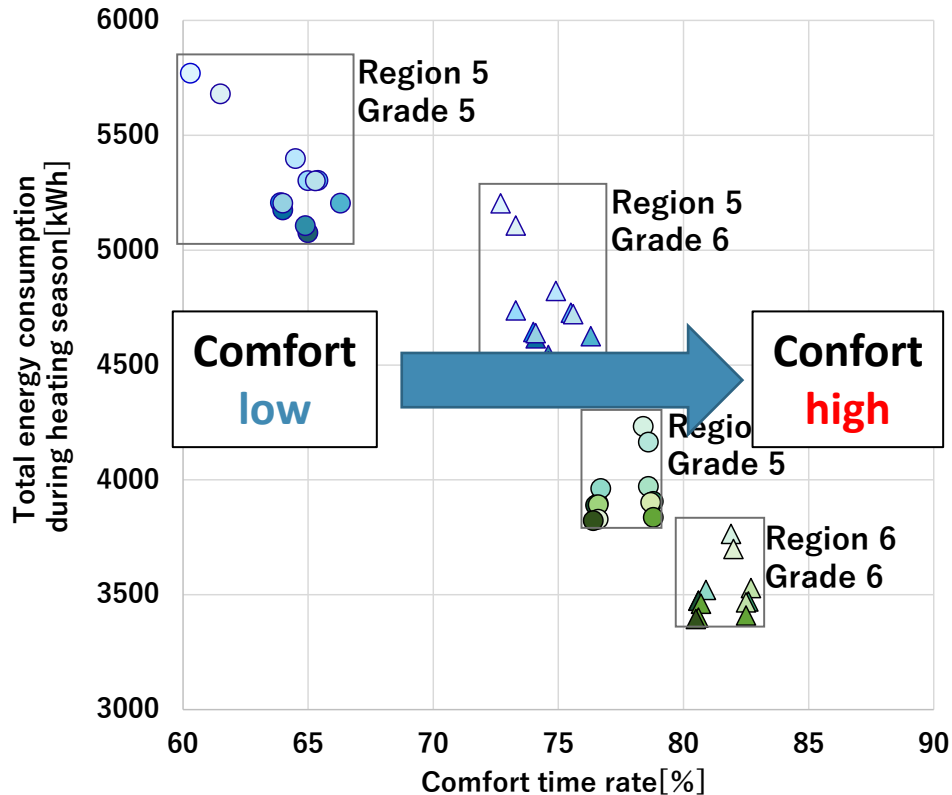


The lower the energy consumption, the higher the energy savings.

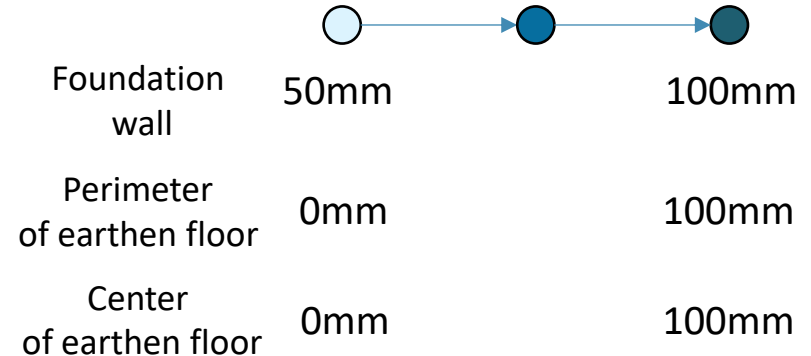
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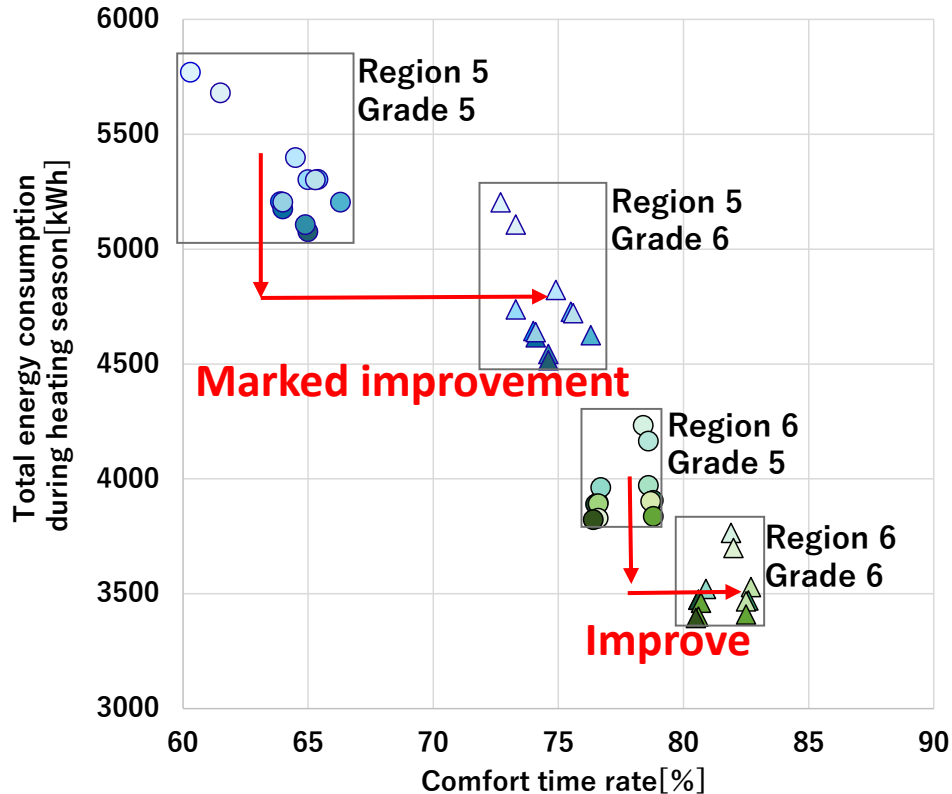


Region 6 is more energy efficient and more comfortable than region 5.

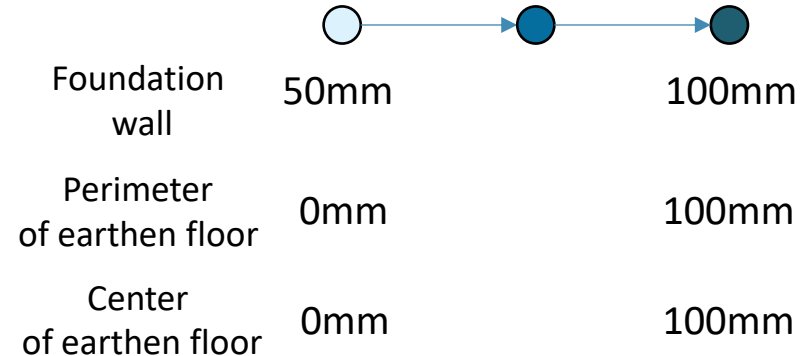
Energy consumption and comfort considerations

$$C_{time} = \frac{OT_{20\sim24}}{d \times 24 \times r} \times 100[\%]$$

C_{time} : Comfort time rate d : Number of days of period covered r : Number of target rooms(Living room, etc.)
 $OT_{20\sim24}$: Number of hours within the target room operating temperature of 20~24° C



- ○ Grade5 △ Grade6
- Blue Region5(Sendai) Green Region6(Tokyo)
- As the insulation becomes thicker, the color is made darker.



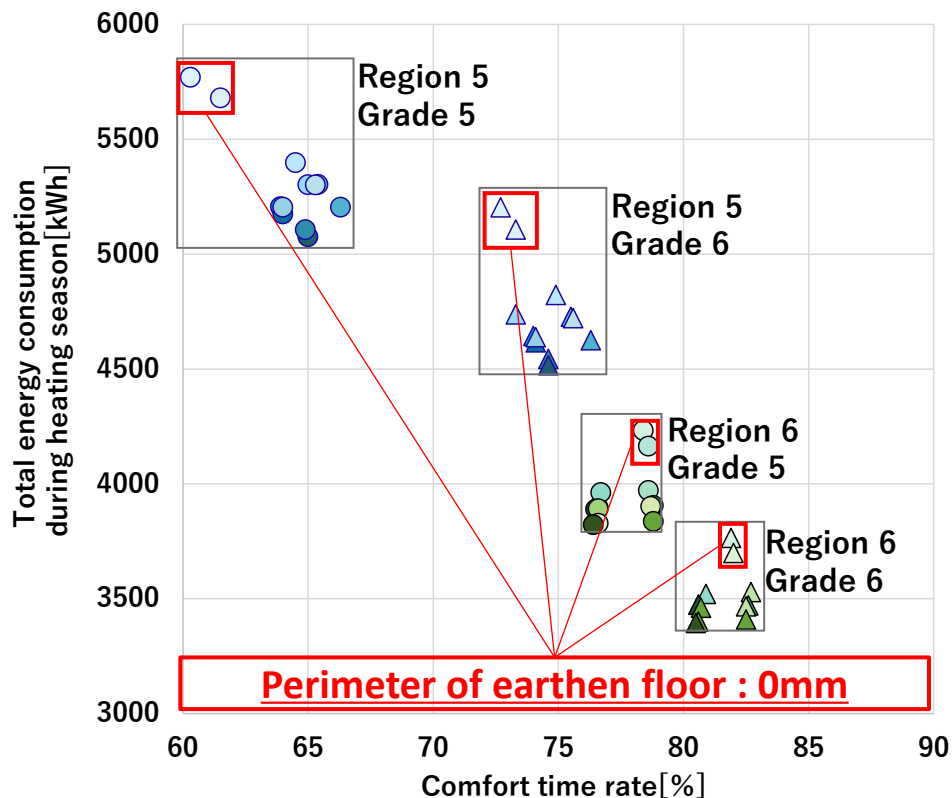
The energy efficiency and comfort improved in both the regions 5 and 6 by changing the insulation grade from 5 to 6.

→ A grade 6 level of insulation is needed in region 5.

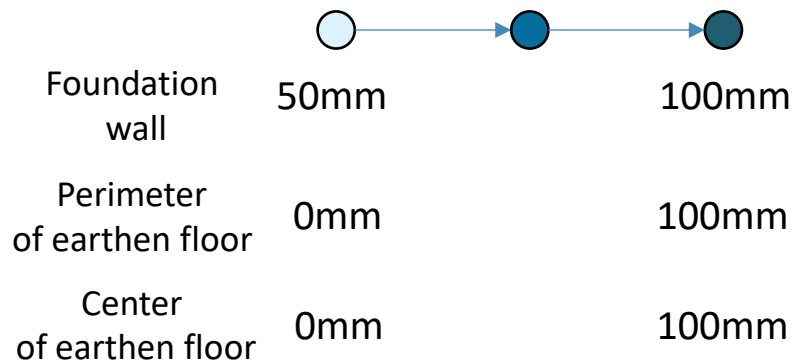
Energy consumption and comfort considerations

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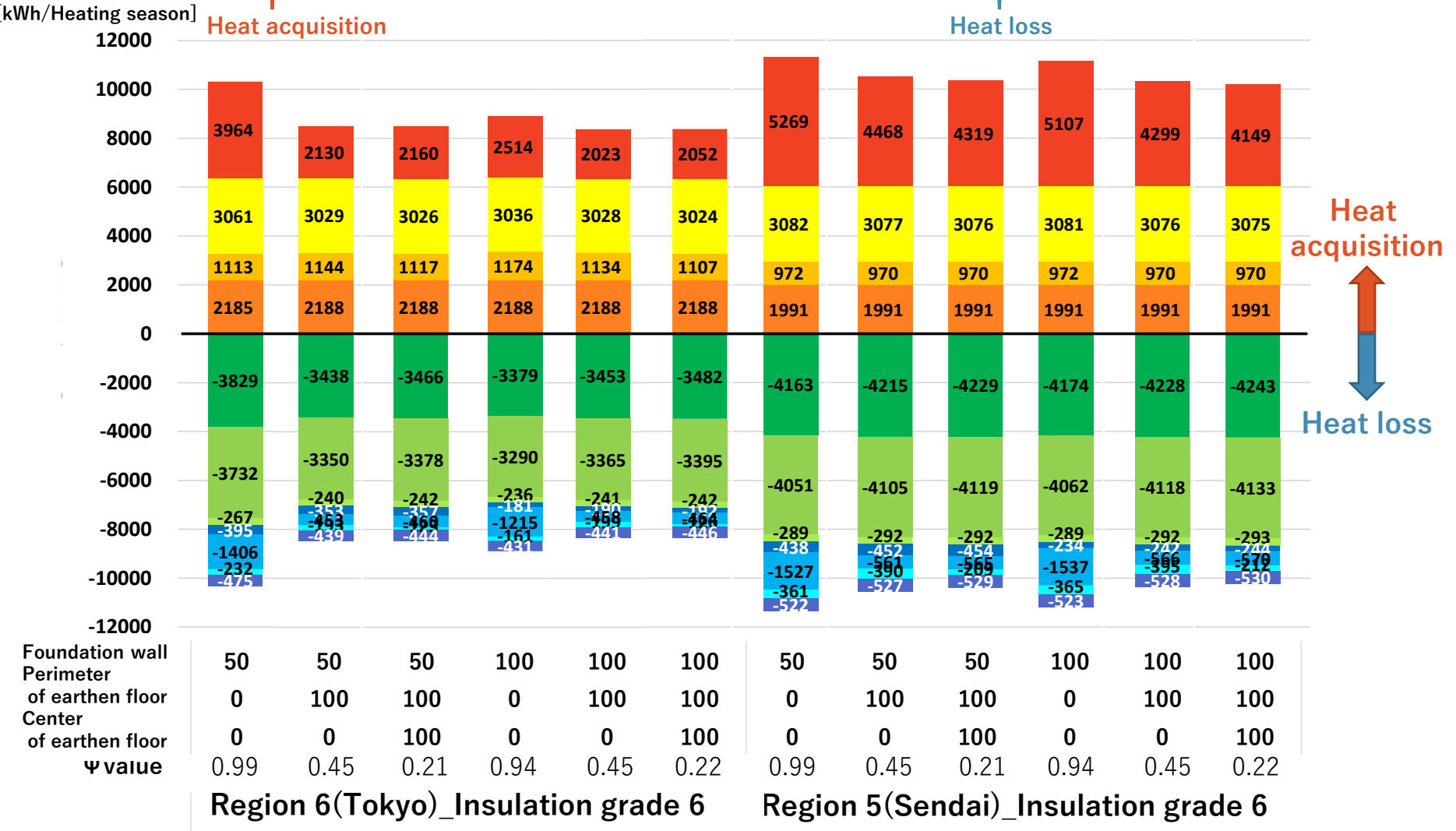


The perimeter of the earthen floor is not insulated, the higher energy consumption in each region and insulation grade, and the lower comfort level especially in region 5.

→ The perimeter of the earthen floor is effective for underfloor heating.

Study of under-floor heat loss

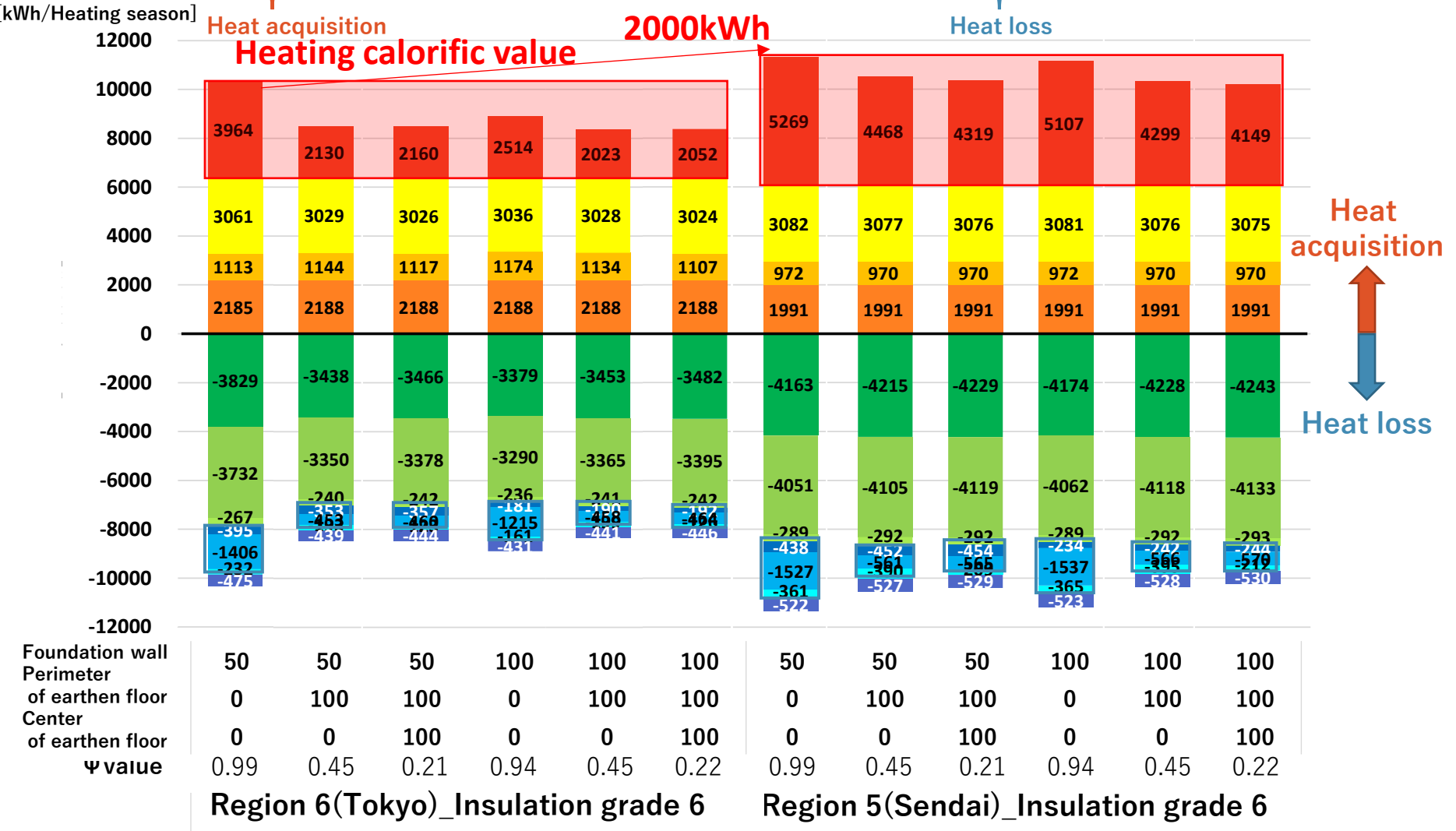
■ Solar heat (aperture)
 ■ Solar heat (wall, roof)
 ■ Internal heat generation
 ■ Heating calorific value
 ■ Aperture
 ■ Wall
 ■ Roof
 ■ Foundation wall
 ■ Perimeter of earthen floor
 ■ Center of earthen floor
 ■ Ventilation



The underfloor heat loss for each case during the heating season (November to April).

Study of under-floor heat loss

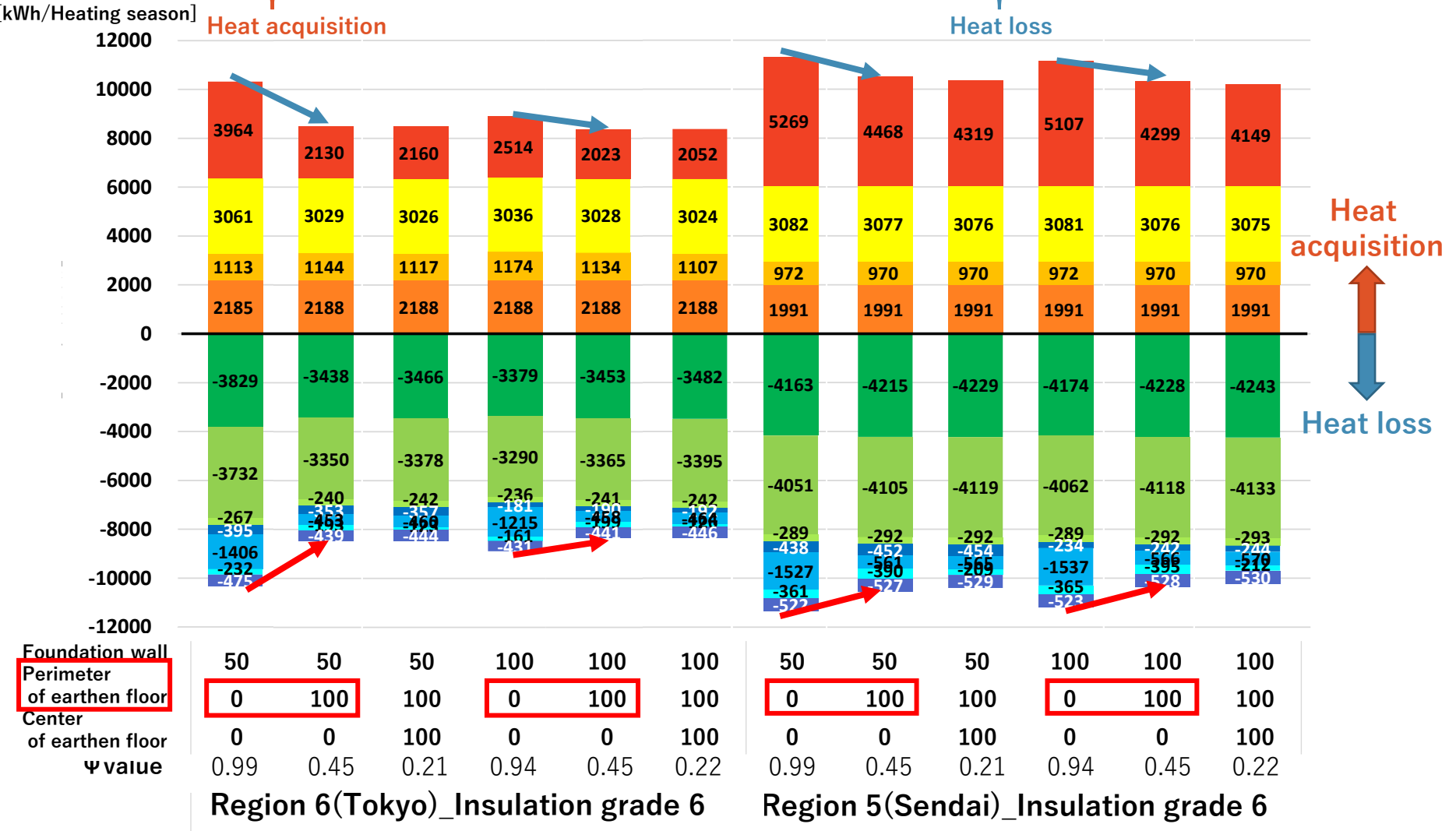
■ Solar heat (aperture)
 ■ Solar heat (wall, roof)
 ■ Internal heat generation
 ■ Heating calorific value
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 ■ Wall
 ■ Roof
 ■ Foundation wall
 ■ Perimeter of earthen floor
 ■ Center of earthen floor
 ■ Ventilation



Compared to region 6, the amount of heating heat increased by about 2000 kWh in region 5.

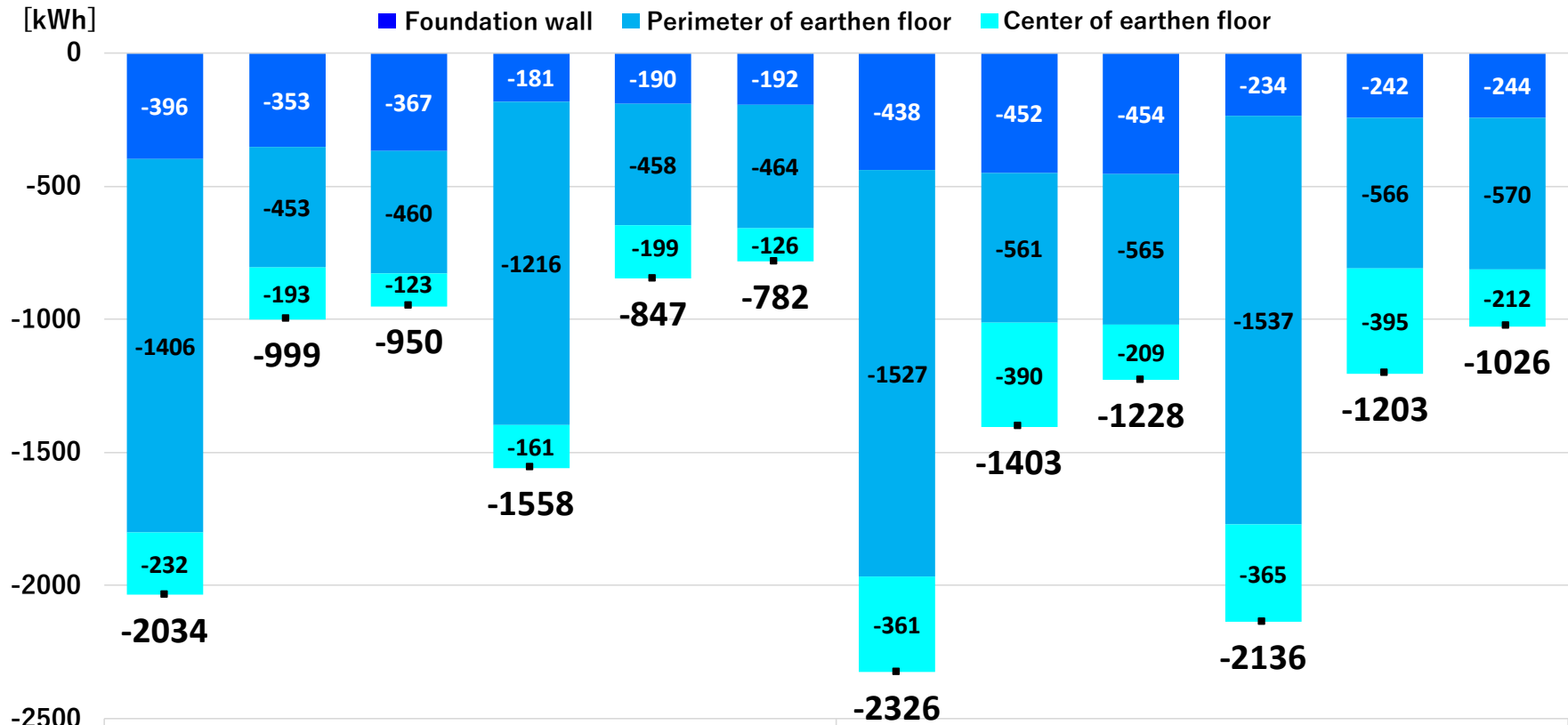
Study of under-floor heat loss

■ Solar heat (aperture)
 ■ Solar heat (wall, roof)
 ■ Internal heat generation
 ■ Heating calorific value
 ■ Aperture
 ■ Wall
 ■ Roof
 ■ Foundation wall
 ■ Perimeter of earthen floor
 ■ Center of earthen floor
 ■ Ventilation



By installing insulation around the perimeter of the earthen floor,
The amount of both heating heat and underfloor heat loss was significantly reduced.

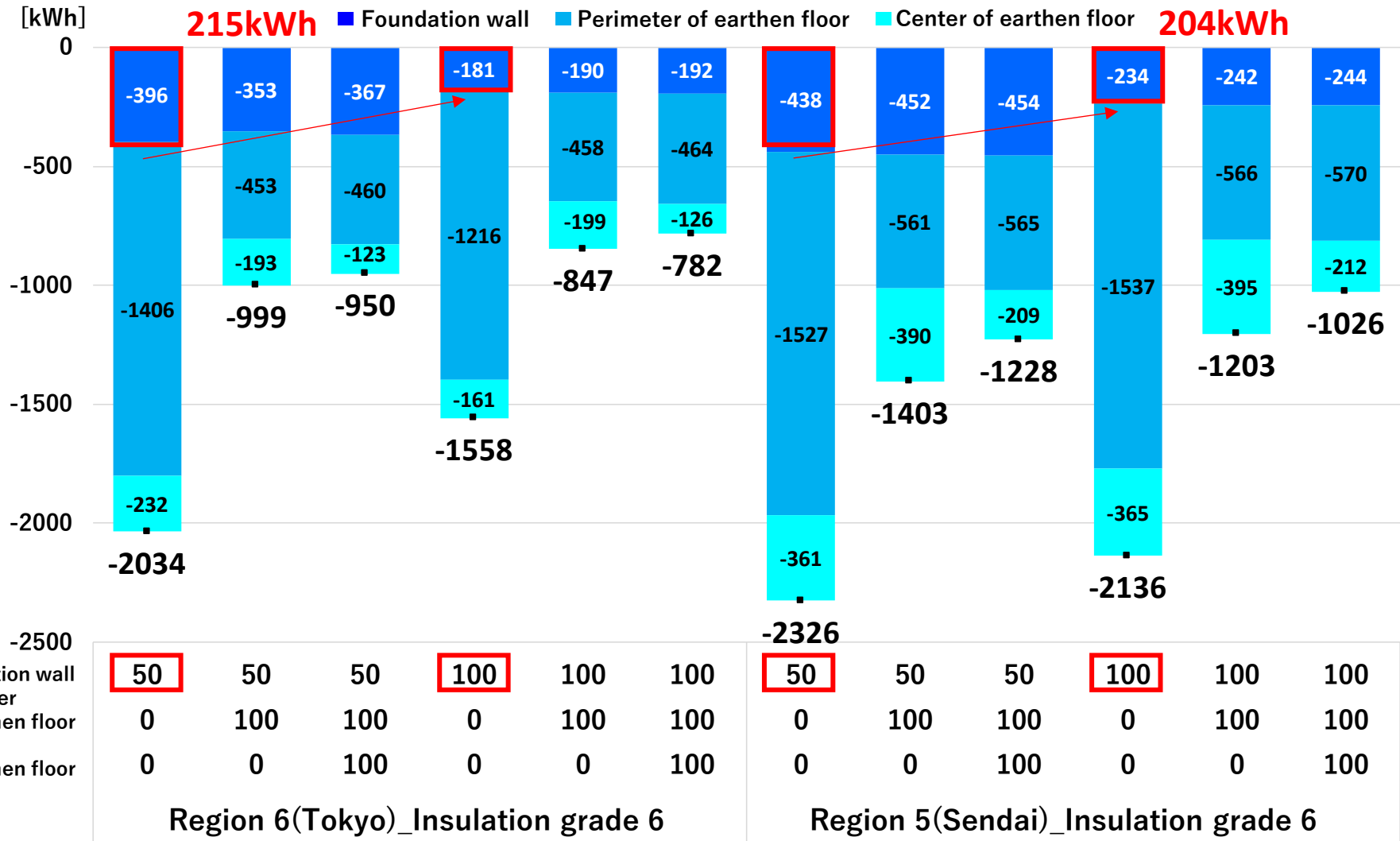
Study of under-floor heat loss



| | | | | | | | | | | | | |
|----------------------------|------------------------------------|-----|-----|-----|-----|-----|-------------------------------------|-----|-----|-----|-----|-----|
| Foundation wall | 50 | 50 | 50 | 100 | 100 | 100 | 50 | 50 | 50 | 100 | 100 | 100 |
| Perimeter of earthen floor | 0 | 100 | 100 | 0 | 100 | 100 | 0 | 100 | 100 | 0 | 100 | 100 |
| Center of earthen floor | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 100 |
| | Region 6(Tokyo)_Insulation grade 6 | | | | | | Region 5(Sendai)_Insulation grade 6 | | | | | |

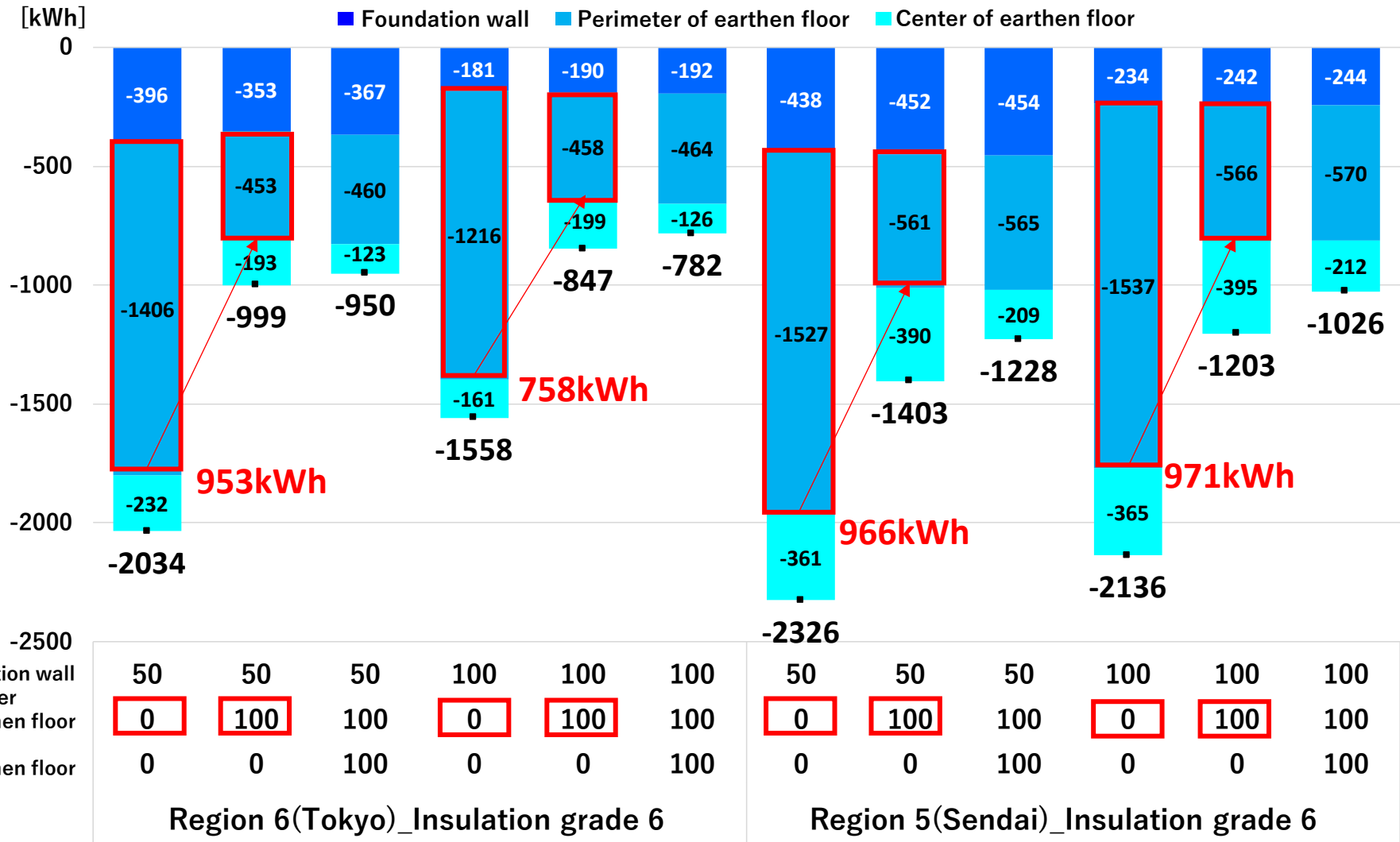
Confirm where foundation insulation can more effectively reduce underfloor heat loss
 : foundation walls, perimeter of earthen floor, or center of earthen floor.

Study of under-floor heat loss



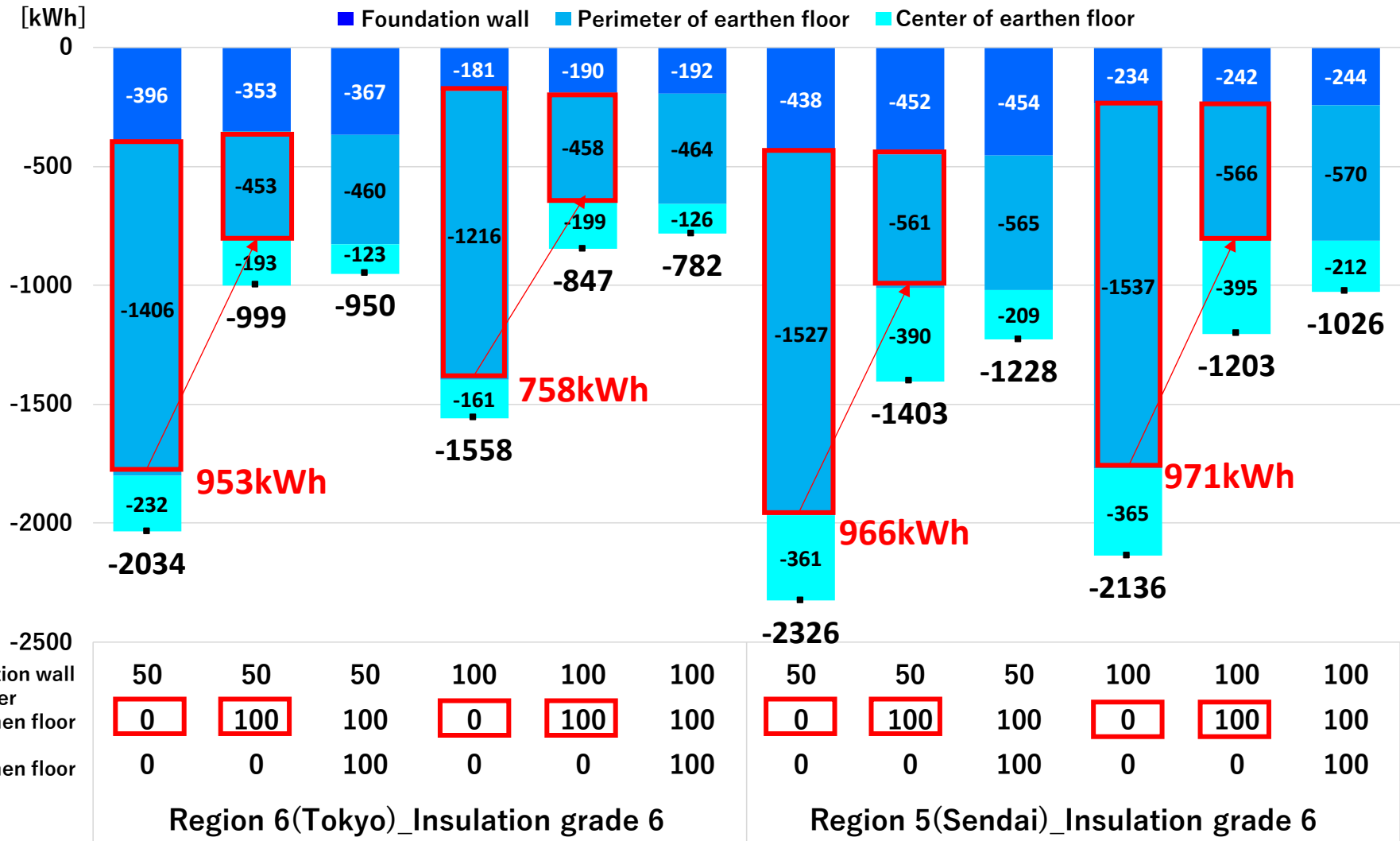
By increasing the thickness of the foundation wall insulation from 50 mm to 100 mm, **the underfloor heat loss decreased by about 200 kWh in each region.**

Study of under-floor heat loss



By increasing the thickness of the perimeter of earthen floor insulation from 0 mm to 100 mm, the underfloor heat loss decreased by about 700~900 kWh in each region.

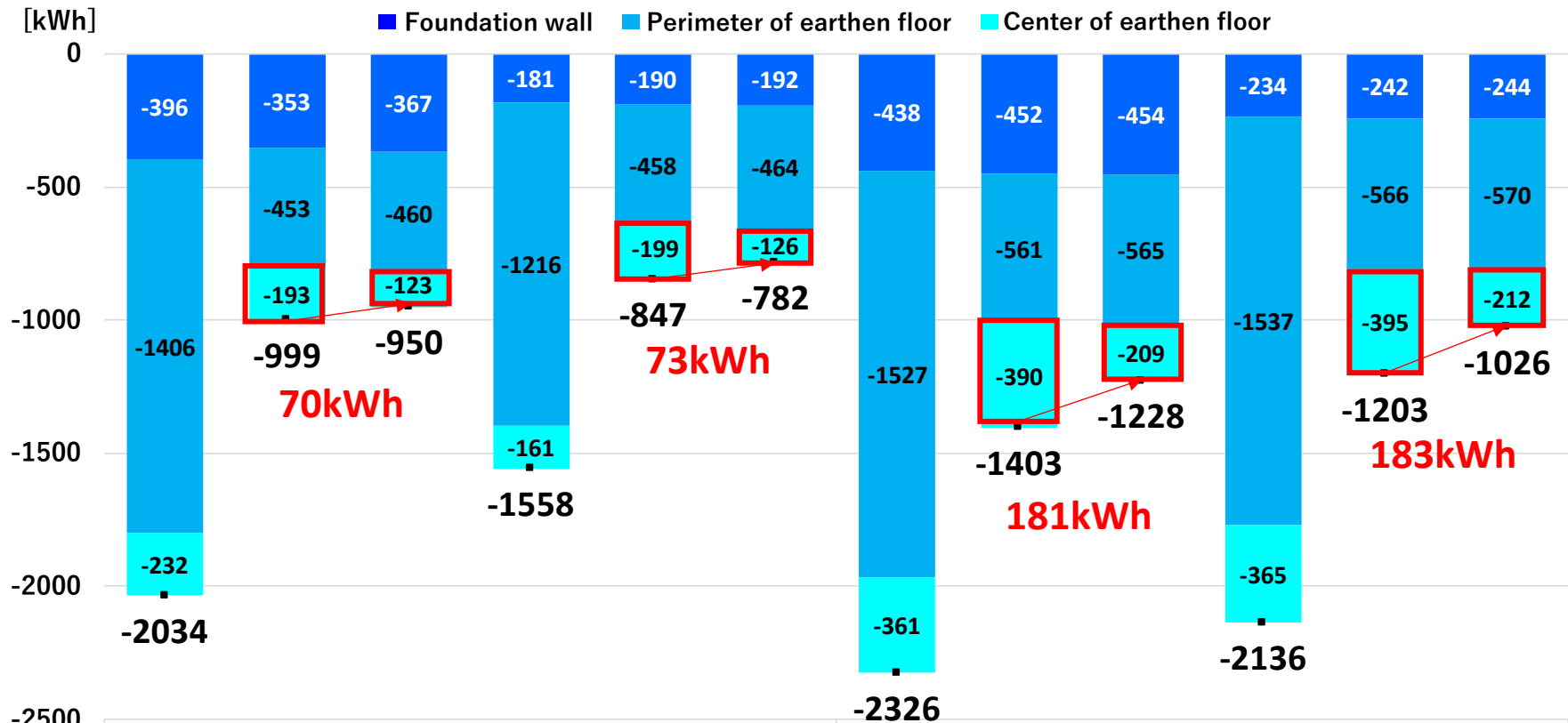
Study of under-floor heat loss



Underfloor heat loss was significantly reduced by installing perimeter of earthen floor insulation.

Demonstrated effectiveness of insulating the perimeter of earthen floor.

Study of under-floor heat loss



| | | | | | | | | | | | | |
|----------------------------|------------------------------------|-----|-----|-----|-----|-----|-------------------------------------|-----|-----|-----|-----|-----|
| Foundation wall | 50 | 50 | 50 | 100 | 100 | 100 | 50 | 50 | 50 | 100 | 100 | 100 |
| Perimeter of earthen floor | 0 | 100 | 100 | 0 | 100 | 100 | 0 | 100 | 100 | 0 | 100 | 100 |
| Center of earthen floor | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 100 |
| | Region 6(Tokyo)_Insulation grade 6 | | | | | | Region 5(Sendai)_Insulation grade 6 | | | | | |

By increasing the thickness of the center of earthen floor insulation from 0 mm to 100 mm, the underfloor heat loss decreased by about 70 kWh in region 6 and 180kWh in the region 5.

Initial and running cost consideration

$$P_{time} = \frac{\text{Construction cost for each insulation specification} - \text{Construction cost for insulation at the base case}}{\text{Heating season electricity charges for the base case} - \text{Heating season electricity rates for each insulation specification}}$$

< The material cost for insulation¹⁾ >

| Type | Item | The lumer cost[yen/m ²] |
|--------------------------|---|-------------------------------------|
| Heat insulating material | High-performance glass wool 10K 100mm | 960 |
| | High-performance glass wool 16K 155mm | 2,140 |
| | High-performance glass wool 24K 120mm | 2,120 |
| | High-performance glass wool 20K 105mm | 2,210 |
| | Phenol foam Class 1 No. 2 63mm | 3,530 |
| | Extruded polystyrene foam Class 3 bA 50mm | 1,623 |
| Aperture | Diagonal move | 54,773 |
| | FIX | 53,424 |
| | Sliding window | 11,817 |

< Calculation of Electricity Rates >

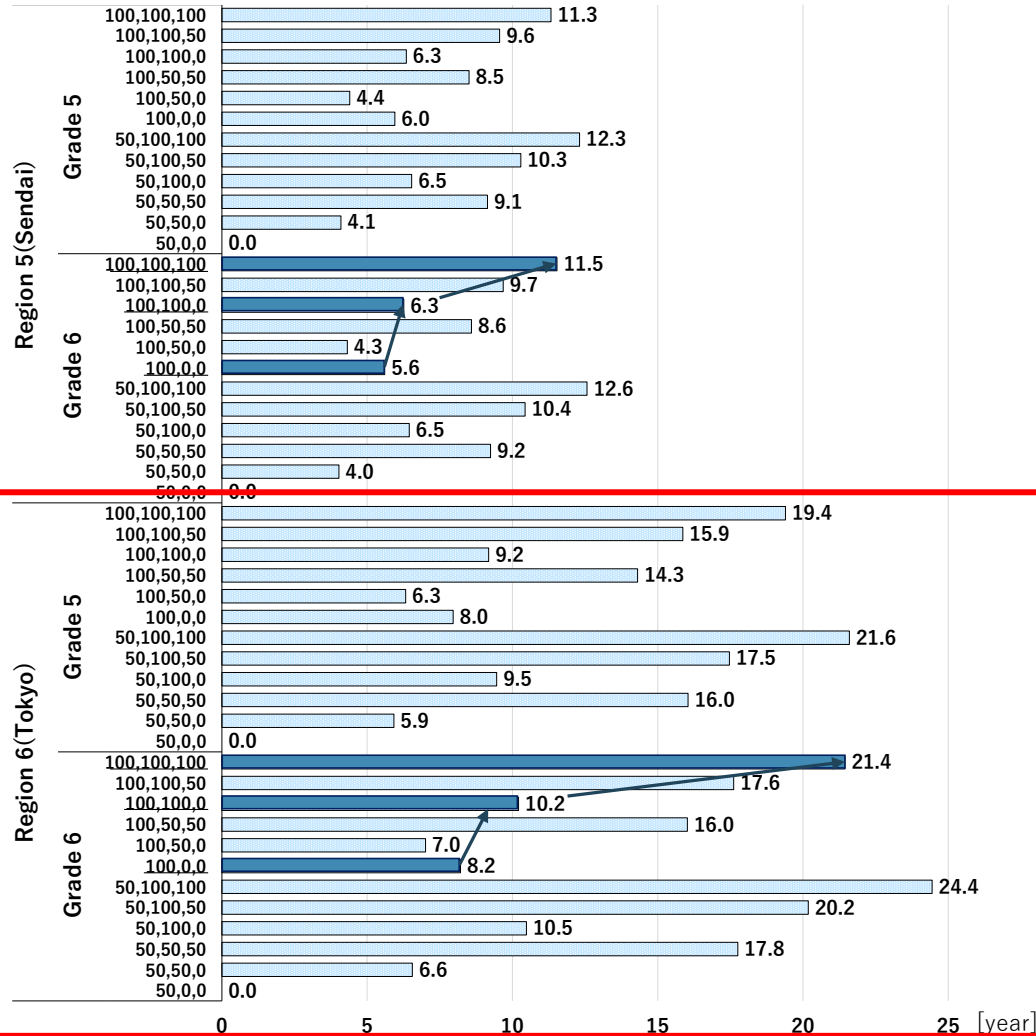
- in consideration of the FIT system, the electricity sales rate is calculated as 16 yen/kWh for the first 10 years, and 8 yen/kWh after the 10th year, when the FIT period ends.
- The purchase price of electricity was set at 40 yen/kWh in consideration of recent electricity prices.

1) Building Construction Research and Development : Accumulation Pocket Notebook, Residential Construction Edition 2021, Economic Research Council, 2021.

Payback time calculation result

$$P_{time} = \frac{\text{Construction cost for each insulation specification} - \text{Construction cost for insulation at the base case}}{\text{Heating season electricity charges for the base case} - \text{Heating season electricity rates for each insulation specification}}$$

Foundation wall, Perimeter of earthen floor, Center of earthen floor

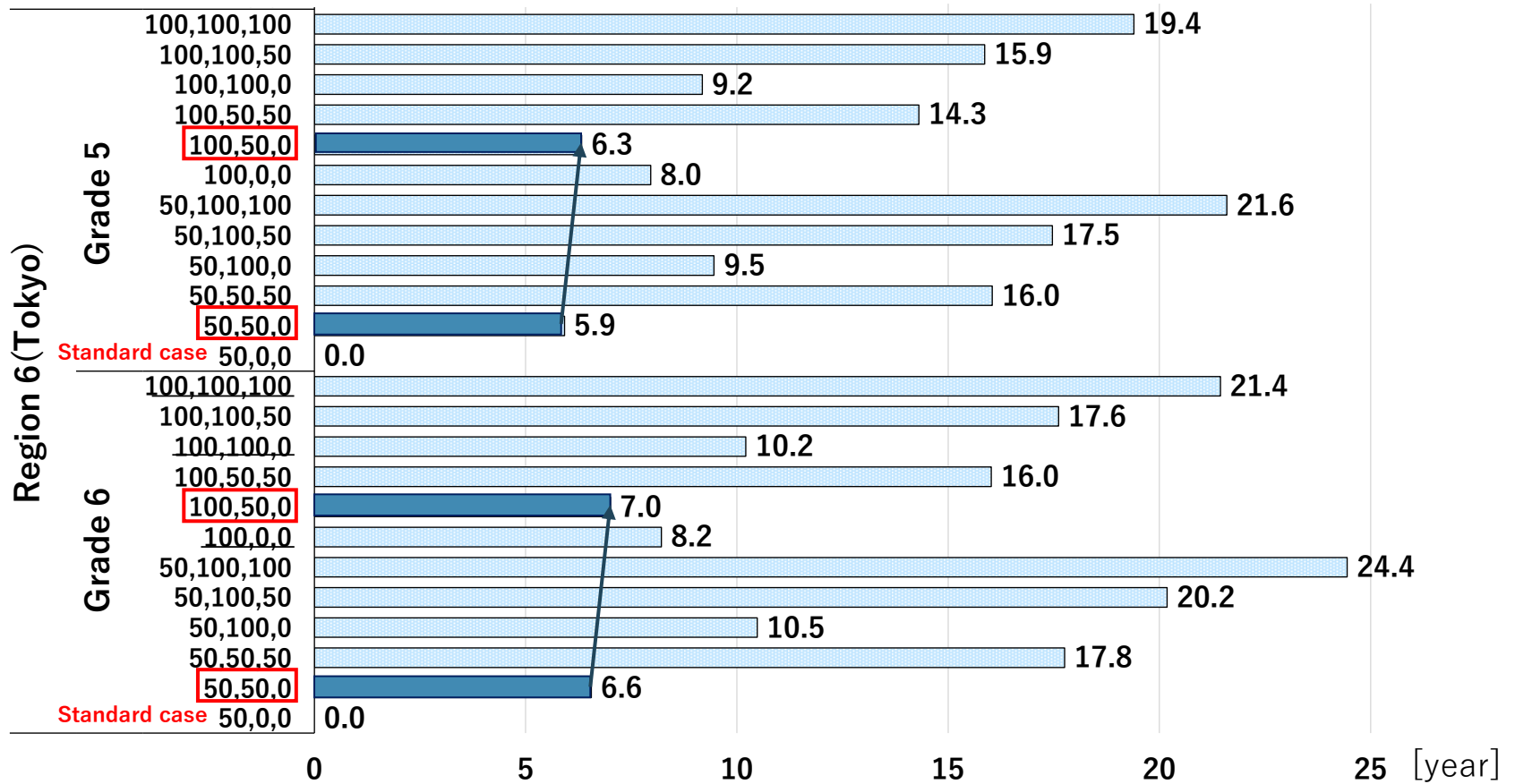


Indicates for Region 6

Payback time calculation result—Region 6(Tokyo)

$$P_{time} = \frac{\text{Construction cost for each insulation specification} - \text{Construction cost for insulation at the base case}}{\text{Heating season electricity charges for the base case} - \text{Heating season electricity rates for each insulation specification}}$$

Foundation wall, Perimeter of earthen floor, Center of earthen floor



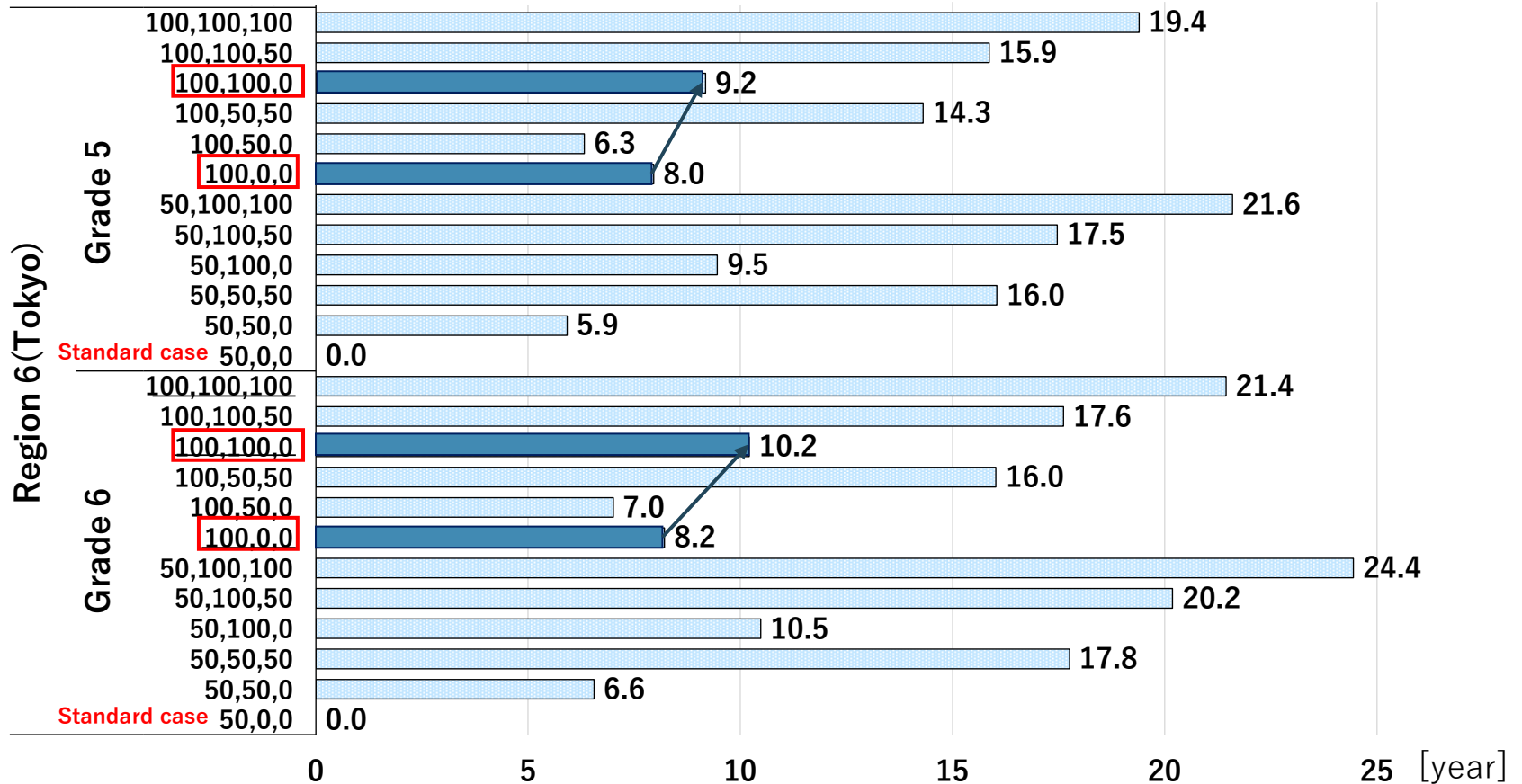
The initial cost could be recovered within one year

when the thickness of the foundation wall insulation material was increased from 50 to 100 mm.

Payback time calculation result—Region 6(Tokyo)

$$P_{time} = \frac{\text{Construction cost for each insulation specification} - \text{Construction cost for insulation at the base case}}{\text{Heating season electricity charges for the base case} - \text{Heating season electricity rates for each insulation specification}}$$

Foundation wall, Perimeter of earthen floor, Center of earthen floor



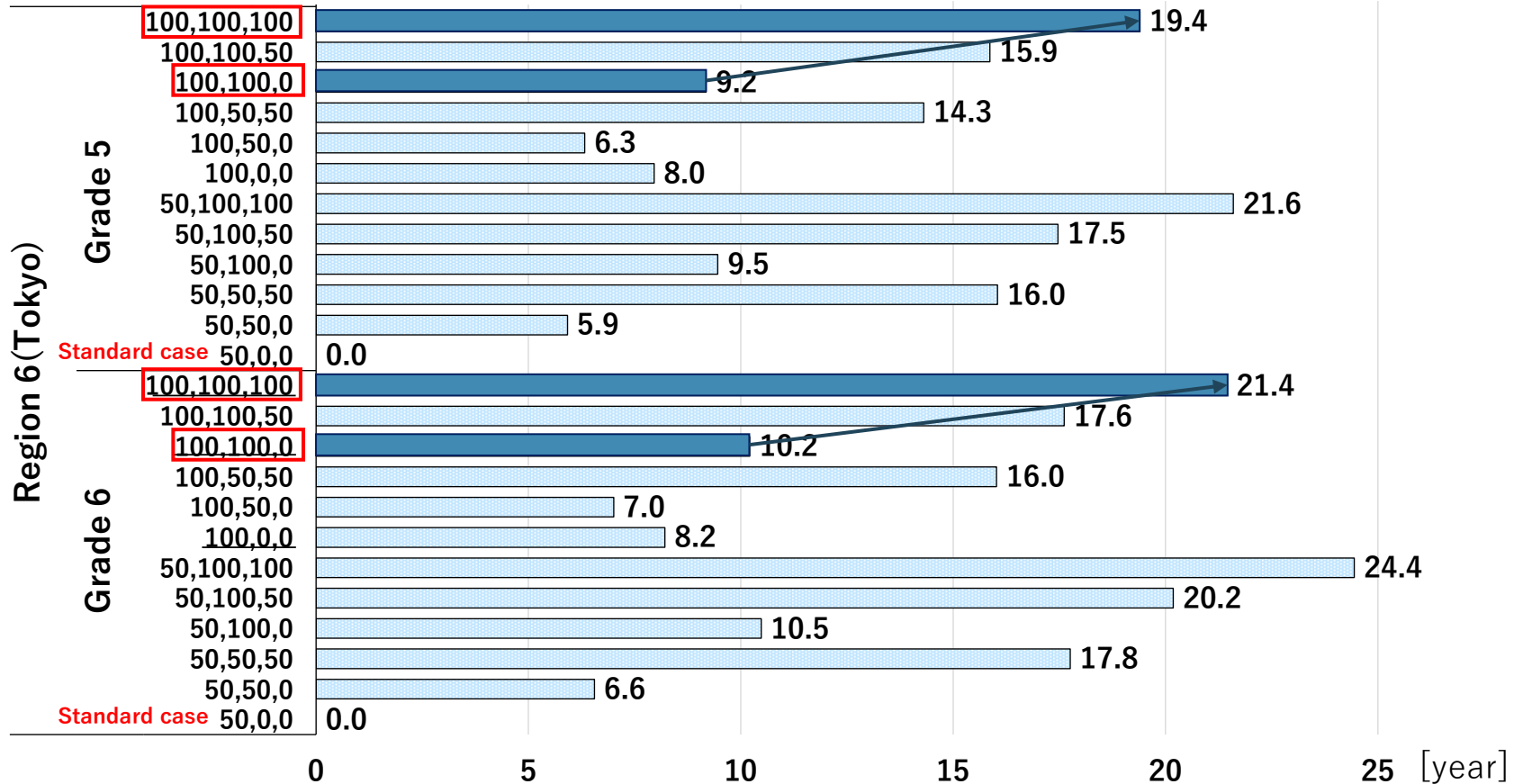
When the insulation thickness of the earthen floor perimeter was increased from 0 to 100 mm, the difference was only about 1 to 2 years.

→The cost-effectiveness of the insulation in the earthen floor perimeter is high.

Payback time calculation result—Region 6(Tokyo)

$$P_{time} = \frac{\text{Construction cost for each insulation specification} - \text{Construction cost for insulation at the base case}}{\text{Heating season electricity charges for the base case} - \text{Heating season electricity rates for each insulation specification}}$$

Foundation wall, Perimeter of earthen floor, Center of earthen floor

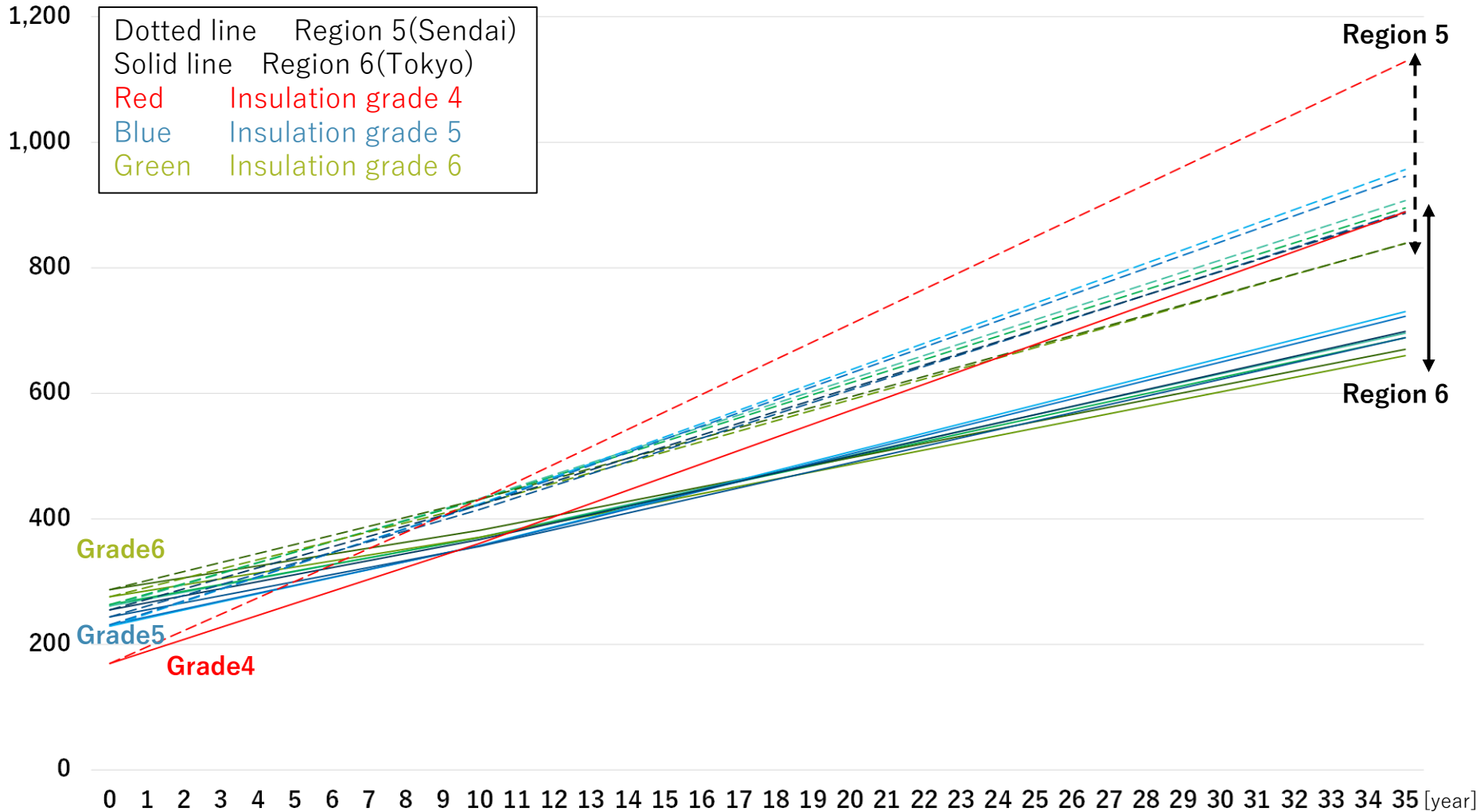


In the center of the earthen floor, when the insulation thickness was increased from 0 to 100 mm, the payback time was longer about 10 years.

The integrated cost transition during the heating period for each insulation performance

Total cost = the initial cost of the insulation work + the running cost during the heating season

[ten thousand yen]

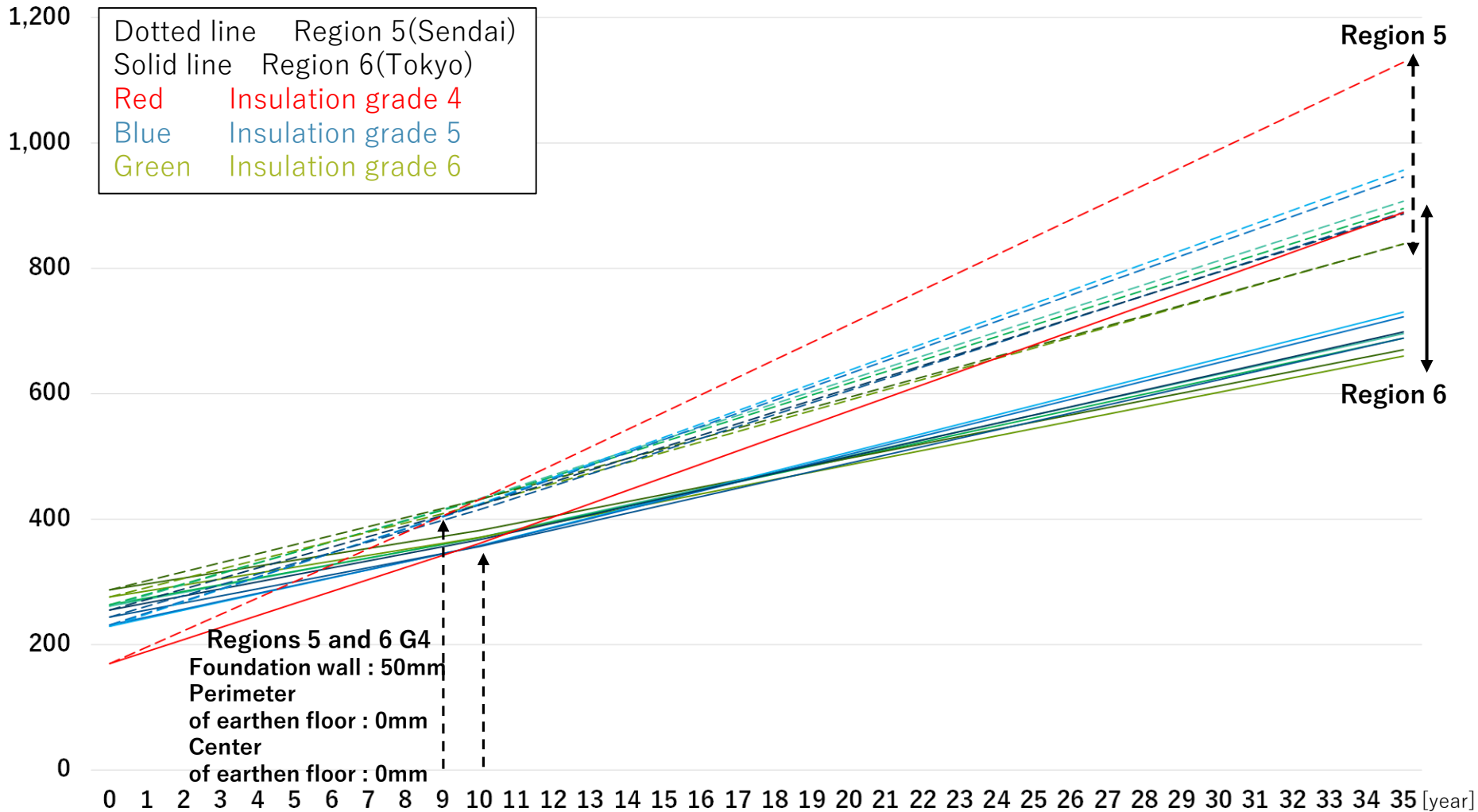


A case of grade 4 (energy conservation standard) was also included in the study.

The integrated cost transition during the heating period for each insulation performance

Total cost = the initial cost of the insulation work + the running cost during the heating season

[ten thousand yen]

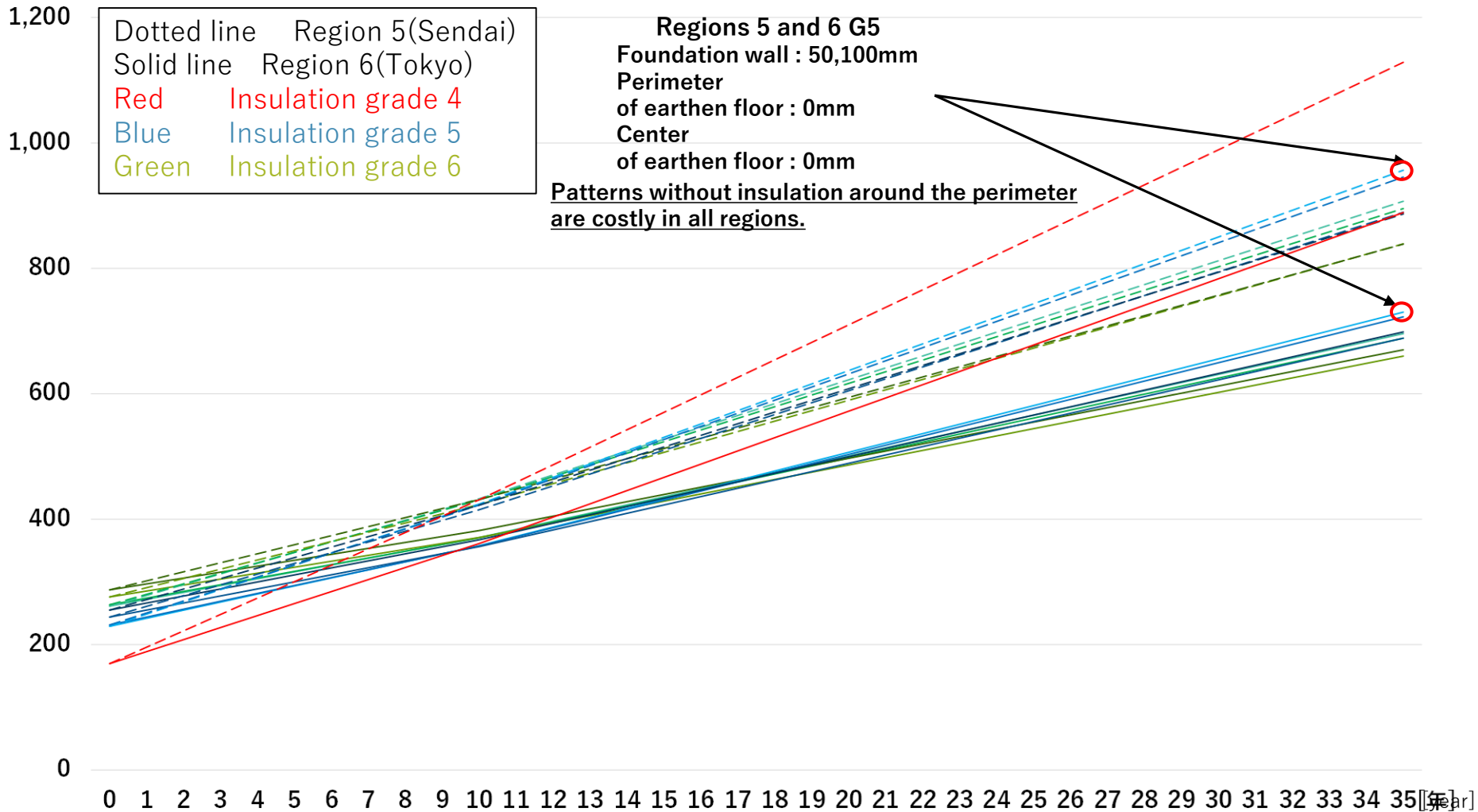


The material and labor costs for insulation work in insulation grade 4 are small, **the total lifetime cost in both regions 5 and 6 are larger than in the other cases after about 10 years.**

The integrated cost transition during the heating period for each insulation performance

Total cost = the initial cost of the insulation work + the running cost during the heating season

[ten thousand yen]

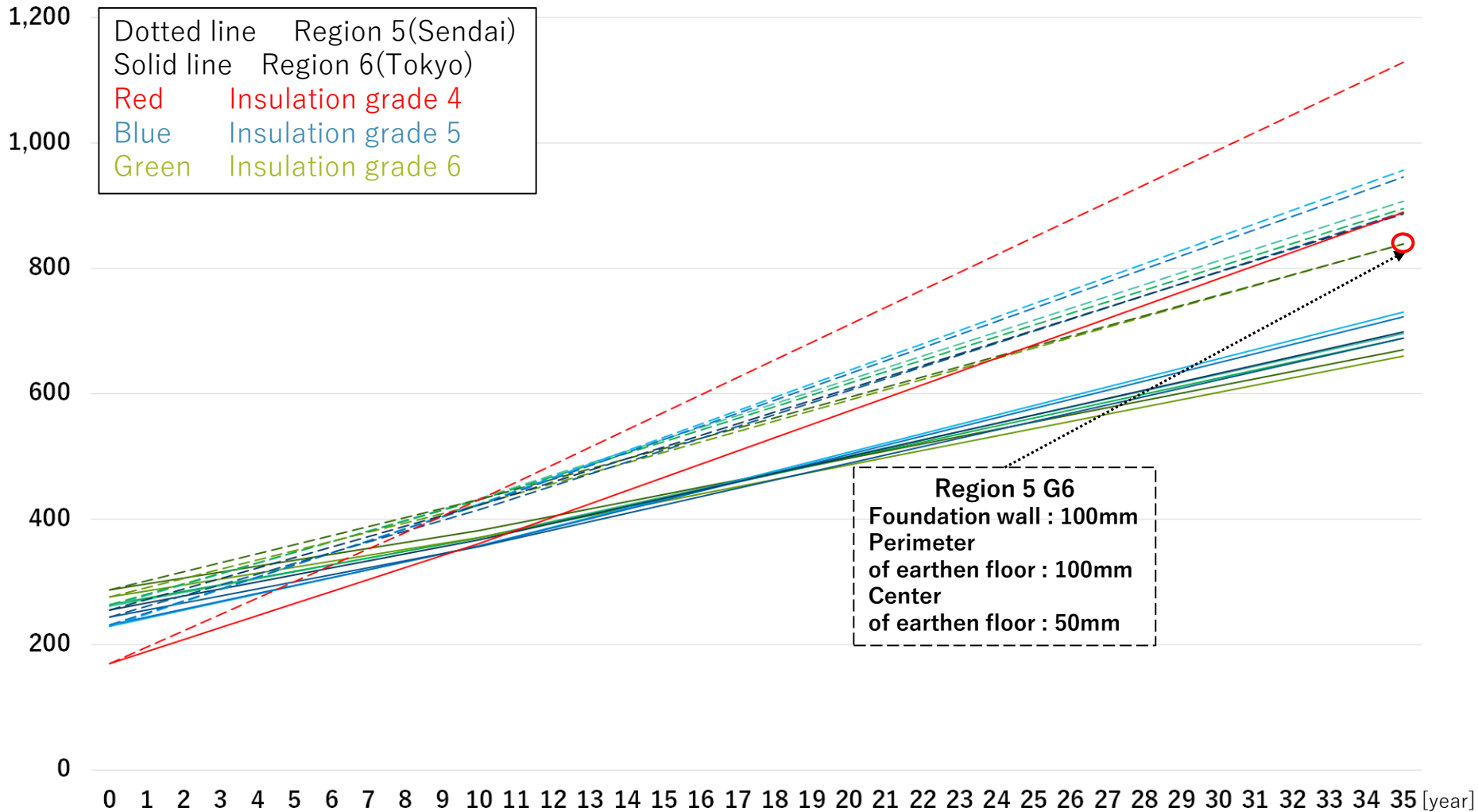


Insulation was not installed at the perimeter and center of the earthen floor, **the lifetime cost was found to be higher in both regions 5 and 6.**

The integrated cost transition during the heating period for each insulation performance

Total cost = the initial cost of the insulation work + the running cost during the heating season

[ten thousand yen]



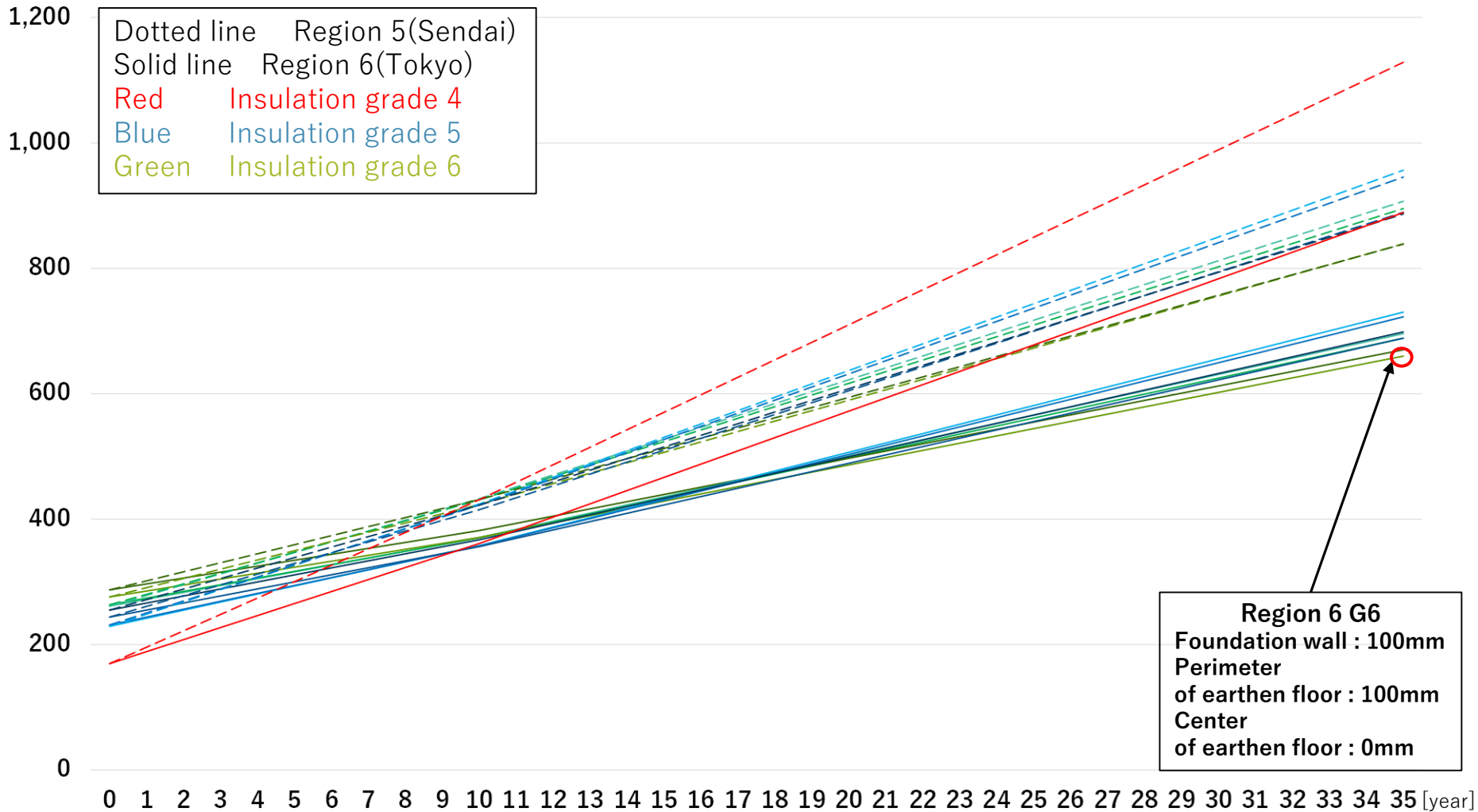
The lowest-lifetime cost insulation specifications in the region 5

Foundation wall → 100mm , Perimeter of earthen floor → 100mm , Center of earthen floor → 50mm

The integrated cost transition during the heating period for each insulation performance

Total cost = the initial cost of the insulation work + the running cost during the heating season

[ten thousand yen]



The lowest-lifetime cost insulation specifications in the region 6

Foundation wall → 100mm , Perimeter of earthen floor → 100mm , Center of earthen floor → 0mm

This study examined the effect of different foundation insulation performance in energy conservation area classifications 5 and 6 used passive standard plans.

Here is what authors found out

- Changing the insulation grade from 5 to 6 in both regions improved energy efficiency and comfort.
- Insulating the perimeter of the earthen floor is effective for underfloor heating.
- The lowest-lifetime cost insulation specifications in each regions.

| Tip | Region 5 | Region 6 |
|----------------------------|----------|----------|
| Foundation wall | 100mm | 100mm |
| Perimeter of earthen floor | 100mm | 100mm |
| Center of earthen floor | 50mm | 0mm |



- **The effectiveness of insulation around the perimeter of the earthen floor was demonstrated in both regions 5 and 6.**
- **In region 5, it was found that the center of the earthen floor should also be laid.**